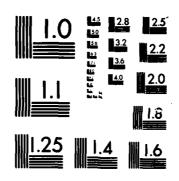
MINUTEMAN STAGE III OPERATIONAL SURVEILLANCE PROGRAM SEVEN-YEAR TESTING B. (U) MORTON THIOKOL INC BRIGHAM CITY UT MASATCH DIV M R KNIGHT DEC 85 TMR-32333 F42600-86-C-0001 F/G 21/9 AD-R164 288 1/2 UNCLASSIFIED F/G 21/9. 2 NL



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Minuteman Stage I Operational Surveil Program Seven-Year Testing Bondline Aging Stu Minuteman Stage III **Operational Surveillance**

Bondline Aging Study

December 1985



MORTON THIOKOL, INC.

Wasatch Operations

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MINUTEMAN STAGE III OPERATIONAL SURVEILLANCE PROGRAM

SEVEN-YEAR TESTING BONDLINE AGING STUDY

DECEMBER 1985

Contract F42600-86-C-0001 DELIVERY ORDER: A003

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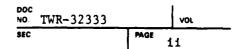


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1.0 INTRODUCTION

This report contains results of the yearly material properties testing of Stage III motor segments in the 12-year bondline aging study. Also reported are the results obtained in the continued testing/monitoring of Motor TC 30024 (LRSLA Simulated Aging Test Motor No. 3), as are the second-year results of tests upon the bondline materials and propellant obtained from dissected Stage III segments of Motor TC 30072. Tests on the excise samples from motors TOP-19, -20, and -21 were not performed this year because the test specimens were not delivered. Figure 1 is a general summary of the tests to be performed.

The testing reported herein was performed during the period of 1 December 1984 through 30 September 1985. The testing of segments from motors TC 30005, TC 30019, and TC 30033 took place during August and September 1985. Second-year tests of the motor TC 30072 segments were conducted in the June-September 1985 time period. The effort was accomplished in accordance with TWR-20946, "Test Plan, Minuteman Stage III Operational Surveillance Program," October 1978, and its Addendum No. 1, dated January 1981, and Addendum No. 2, May 1983.

1.1 Twelve-Year Bondline Aging Study

This phase of the Minuteman Stage III Surveillance Program uses segments removed from three in-process reject motors: TC 30005, TC 30019, and TC 30033. All three motors were cast in 1971 and were rejected due to apex voids. Segments maintained at silo conditions are being used to track bondline aging of Stage III motors with testing of material properties being performed at one-year intervals to 1990. This report contains the data from the seven-year aging test interval. The actual time between baseline or zero-time testing and this test period is about 78 months.

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1.2 Testing/Monitoring of Motor TC 30024

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Motor TC 30024 was earlier conditioned for 16 months at 110°F and 80 percent RH as LRSLA Simulated Aging Test Motor No. 3, wherein the liner at the forward flap was brought to a fully degraded condition. Between the end of conditioning and August 1981, a period of 23 months, motor TC 30024 was kept in storage in a horizontal position at approximately 70°F and ambient RH. Since then, it has been in vertical storage, aft end down, at 70°F and 50 percent RH interrupted only for brief periods to allow radiographic and visual inspection at regular intervals to monitor the existing forward and aft bondline separations and other areas of the motor. In addition, motor TC 30050 segments that accompanied this motor during the Simulated Aging Test are being tested at two-year intervals (in 1981, 1983, and 1985) to give an indication of the present material properties of motor TC 30024.

1.3 Material Properties Testing of Dissected Motor TC 30072

Motor TC 30072 was cast on 8 December 1971, spent most of its life in the operational force, and then was fully dissected by Wasatch Operations personnel during April and May 1983. Following dissection, extensive material properties testing of the propellant/liner/insulation bond system was performed on motor segments from preselected locations. The remaining motor segments will be tested at one-year intervals over the next five years. Prior to testing, the segments are being stored at nominal silo conditions. The second-year test results are reported herein, representing the motor condition at about 165 months of age.

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2.0 OBJECTIVES

2.1 Twelve-Year Bondline Aging Study and Excise Sample Testing

The program objective is to provide material properties aging data at silo conditions (70° + 5° F, 50 + 5 percent RH) for liner bond strength,

ANB-3066 propellant, SD-851-2 liner, and V-45 insulation from selected locations of three Minuteman Stage III motors. These data are to be used to relate the conditions of the dissected motors to those of operational motors (via excise samples) and to compare and adjust the age of all of these to the Stage II nominal liner degradation curve.

2.2 Testing/Monitoring of Motor TC 30024

The monitoring of motor TC 30024 and testing of accompanying motor segments are intended to determine if continued storage of motor TC 30024 will result in the worsening or healing of the liner condition and existing bondline separations in the motor.

2.3 Material Properties Testing of Dissected Motor TC 30072

The dissection of a Stage III motor from the operational force and testing of its material properties are intended to allow verification of motor aging predictions related to liner degradation by a determination of the longitudinal and circumferential bond strength profiles. Measurement of the bore surface propellant properties is used to verify satisfactory strain capability.

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3.0 SUMMARY AND CONCLUSIONS

3.1 Twelve-Year Bondling Aging Study

Testing for the seven-year interval was performed on the forward flap and forward equator motor segments. As in the earlier test intervals, the results and trends were confirmed. The propellant/liner/insulation bond strength continues to decline with motor age. The rate of decline in the forward flap area has slowed with the mini DPT bond strength being about 34 psi. The decline in the forward equator was much greater than previous values, being down to approximately 51 psi from last year's value of 64 psi. A continuing increase in liner swell ratios and decline in liner gel fraction are further evidence of continued liner degradation. An additional decline in the relaxation modulus of propellant, particularly immediately adjacent to the liner interface, is again noted. Increases in the separation from termination in the bore to the aft flap hinge were observed. Separations at the 300 to 330 degree locations showed no appreciable changes, while inspection of the 20 to 290 degree motor locations show increases of +6 to +10.1 inches from the 64-month data.

3.2 Testing/Monitoring of Motor TC 30024

The visual and radiographic inspections of motor TC 30024 reveal moderate changes in the condition of the propellant/liner/insulation bondline during approximately two years of storage and monitoring at silo conditions.

3.3 Material Properties Testing of Dissected Motor TC 30072

Material properties of motor TC 30072 show the same trends as the three surveillance dissect motors. Liner degradation is evidenced by a decrease in mini DPT bond strength, increase in liner swell ratio, and decrease in

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liner gel fraction. The bond strength (see Tables 32 to 37) follows the usual trends of being highest near the equator, lowest in the flap areas, and much better under and between the grounding straps.

Stress relaxation data for the propellant near the liner interface show a correlation between liner bond strength and relaxation modulus. The higher the bond strength, the higher the relaxation modulus.

Material properties of V-45 insulation from various motor locations were determined. The relaxation modulus is higher in the equator areas and lower near the flaps. V-45 swell ratios appear to be similar at all motor locations tested. V-45 moisture analysis showed a greater increase in percent moisture in the aft flap and forward equator regions with moisture content being lowest in the barrel area, between and under the grounding straps.

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4.0 METHOD

4.1 Material Properties Testing

Insofar as possible, all testing of motor segment or excise sample material properties throughout the bondline study has been carried out in a uniform fashion and according to the following test methods.

4.1.1 Segment Sampling

The foil/epoxy seal and any interfering fiberglass case material is removed from the motor segments prior to test sample preparation using these procedures:

DP 2413-018, Cutting of Stage III Minuteman Segments for Lab Sample Preparation

DP 2413-021, Minuteman Stage III Fiberglass Case Removal From Motor Segments by Grit Blasting

4.1.2 Mechanical Property Test Methods

4.1.2.1 Mini DPT Bond Tensile

DP 2413-008, Preparation of Mini Double Plated Tensile (Mini DPT) Bond Strength Specimens

DP 2413-013, Testing of Mini Double Plated Tensile (Mini DPT) Bond Strength Specimens

4.1.2.2 Propellant Relaxation Modulus

DAP 0270, Determination of Relaxation Modulus of Propellant by Use of Mini Tensile Specimens

DP 2413-015, Stress Relaxation Testing Using the Instron Tensile Tester

4.1.2.3 Shore A Hardness (15-Second)

SOP 325, Section 6

4.1.2.4 Propellant Mini Tensile

SLP-528, Mechanical Forming of Propellant Specimens

DP-2413, Operation of Instron Tensile Testing Instruments

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4.1.2.5 V-45 Relaxation Modulus

LTP-2413-0151, Preparation of Rubber Stress Relaxation Specimens from Motor Segments

DP 2413-015, Stress Relaxation Testing Using the Instron Tensile Tester

4.1.2.6 SD-851-2 Liner Relaxation Modulus

SLP-472, Penetrometer Hardness Testing of Liner Propellent Bond

- 4.1.3 Chemical Property Test Methods
- 4.1.3.1 SD-851-2 Liner Moisture

 DAP 0269, Determination of Moisture in SD-851-2 Liner
- 4.1.3.2 SD-851-2 Liner Solvent Swell Ratio

DAP 0197, Determination of Solvent Swell Ratio of Cured Liner from MM III Stage Samples

4.1.3.3 SD-851-2 Liner Gel Fraction

DAP 0254, Determination of Minuteman III Stage Liner Gel Fraction

- 4.1.3.4 V-45 Moisture Content
- 4.1.3.4.1 Azeotropic Distillation

DAP 0321, Determination of Moisture in Rubber by Azeotropic Distillation

4.1.3.4.2 DuPont Moisture Analysis

DAP 0317, Determination of Moisture in V-45 and C-4 Insulation by DuPont Moisture Evolution Analyzer

4.1.3.5 V-45 Swell Ratio

DAP 0197, Determination of Solvent Swell Ratio of Cured Liner from MM III Stage Samples

4.1.3.6 V-45 DOP Content

DAP 0300, Determination of DOP in V-45 Rubber

4.1.3.7 SD-851-2 Liner C=O/C=C Absorbance Ratio

DAP 0399. Infrared Analysis Using the Nicolet 7199 FTIR

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4.1.4 Evaluation of Material Properties Test Results

Once the testing of the motor segments was accomplished, results were compared with those from earlier test intervals or other aging and surveil-lance motors. This was done largely through the use of plots of measured values versus conditioning time or motor location.

4.2 Twelve-Year Bondline Aging Study

As at earlier test intervals, the designated segments (see Figure 2 and Table 1) were removed singly from conditioning, the foil/epoxy seal was removed, and lab specimens were prepared and tested in accordance with Table 2 and the above cited methods. While awaiting testing, the specimens were kept tightly sealed in aluminum foil to minimize loss of moisture.

4.3 Testing/Monitoring of Motor TC 30024

Simulated silo conditioning of motor TC 30024 at $70^{\circ} \pm 5^{\circ}$ F and $50 \pm 5^{\circ}$

Additional information as to the present condition of the bondline and propellant in motor TC 30024 is being obtained by periodic testing of the material properties of segments from motor TC 30050 (see test matrix in Table 24). These segments accompanied motor TC 30024 throughout the LRSLA SAT conditioning, and in that accelerated aging test, motor TC 30050

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segments were laboratory tested to verify that the liner in the forward flap region of the intact motors, TC 30024 and TC 30106, was fully degraded. The first testing of these segments under the surveillance program was performed in September 1981, after additional storage with motor TC 30024 at silo conditions for about 1.5 years. All tests at the present and at earlier times were performed in accordance with the test procedures cited in Section 4.1.

4.4 Material Properties Testing of Dissected Motor TC 30072

The full dissection and material properties testing of Stage III motors from the operational force was first proposed in 1981¹, but the first such motor, TC 30072, did not become available until early 1983. With its availability came a request that the test plan be revised to provide for additional material properties testing to track the bondline condition to at least 17 years of motor age. Without making changes in the original dissection plan or deleting any of the originally planned material properties testing, the test plan was revised². The current plan makes use of motor segments that would have otherwise gone unused and provides for annual testing to 1989 (Table 28), or about 17.5 years of age for motor TC 30072.

Following dissection of motor TC 30072 by Operations personnel, further subsectioning of the motor segments and preparation and testing of laboratory specimens was performed by workers in the Research and Development Laboratories. This testing was performed in accordance with the methods cited above, and results are presented in Section 5.2.

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¹TWR-20946, "Test Plan, Minuteman Stage III, Operational Surveillance Program, Addenum No. 1," January 1981.

²TWR-20946, "Test Plan, Minuteman Operational Surveillance Program, Addendum No. 2," May 1983.

5.0 RESULTS

5.1 Twelve-Year Bondline Aging Study

The plan for motor segment use and the material properties test matrix for the 12-year (1978 to 1990) bondline aging study using motors TC 30005, TC 30019, and TC 30033 are shown in Tables 1 and 2. The motor segment layout is in Figure 2. The results of the material properties testing at the seven-year test interval (actually 76 months of conditioning at 70°F and 50 percent RH) are summarized in Figures 3 to 24 and Tables 3 to 22. In the latest testing, only the forward flap and forward equator segments were tested, as planned. Earlier trends and results tend to be confirmed. As noted in previous test intervals, the motor-to-motor differences in general are small.

The propellant/liner/insulation bond tensile strength continues to drop off with increasing motor age or conditioning time. At the 76-month interval, the bond strength (34 psi) is approximately the same as the 64-month data in the forward flap area (see Figure 3). In the forward equator, bond strength has dropped from 64 psi at 64 months to 51 psi at 76 months. In the forward flap area, the liner swell ratio has increased to a value of 2.13, and the liner gel fraction has decreased to a value of 0.40. These results confirm that degradation continues to be least in the most protected locations, that is where moisture enters with difficulty, as at the forward equator and two inches aft of the forward equator.

Propellant relaxation modulus has declined with storage time, particularly immediately adjacent to the liner interface. This effect can be caused by moisture effects and migration of DOP plasticizer from the V-45 insulation: the amount of contribution of each to the degradation has not been identified.

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5.2 Testing/Monitoring of Motor TC 30024

5.2.1 Motor Inspection

Radiographic inspections of motor TC 30024 revealed evidence of further liner degradation in some areas while other areas showed no appreciable change. More degradation was evident in the flap bulb area. The separations that were found between the aft polar boss insulation and glass at the aft tip have not changed. There was also no evidence of change in the forward flap area. However, new separations from the in bore to 12 inches aft of the aft flap bulb hinge were detected in Area A at 172 deg angular location.

Visual inspections of motor TC 30024 have shown no trends in the physical measurements to indicate significant changes in either the motor bore diameter or the forward gap area. There is also no apparent hardening of the propellant surface in the aft bore. The latest Shore A readings ranged from 74-79, slightly lower than values for August 1981.

5.2.2 Segment Testing

The results of material properties testing of the motor TC 30050 segments that have accompanied motor TC 30024 since the LRSLA Simulated Aging Test conditioning are summarized in Figures 26 to 32 and Tables 25 to 27. The bond strength and liner gel fraction show a slight decrease in values as compared to baseline data. Liner swell ratios also follow a similar trend with a slight increase in swell ratio values.

5.3 Material Properties Testing of Dissected Motor TC 30072

The plans for baseline and later testing of the material properties of dissected operational motor TC 30072 are shown in Tables 28 to 31. The designation of specific motor segments is obtained from Figures 34 to 39. The results of the 1985 material properties testing are summarized in Figures 40 to 62 and Tables 32 to 48.

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5.3.1 Bond Strength and Liner Properties

The motor TC 30072 propellant/liner/insulation bond strength and liner properties test results are summarized in Figures 40 to 48 and Tables 32 to 37.

The effects of motor location and crosshead test rate on mini DPT bond strength are seen in Figures 40 and 41. The bond strength is highest in the barrel region and near the equators where there is the lowest moisture penetration. Also evident is the existence of lower bond strength in the forward end of the motor than in the aft end. The motor profiles of liner gel fraction and liner swell ratio show a trend for a decrease in gel fraction and increase in swell ratio values. Liner swell ratio values show a decrease in the more protected barrel region.

5.3.2 Relaxation Modulus of Propellant at the Bondline

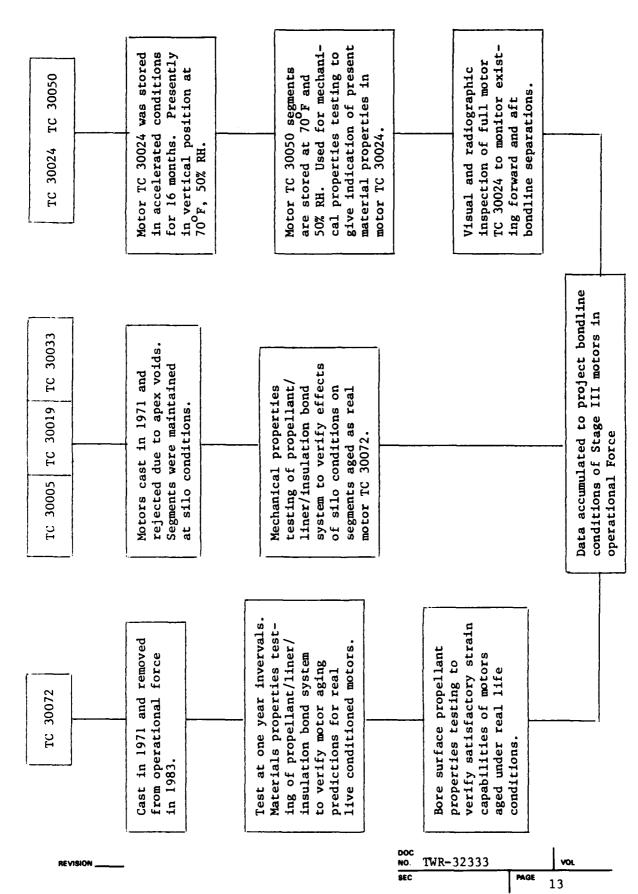
Stress relaxation testing results for motor TC 30072 are shown in Figures 49 to 61 and Tables 38 to 45. The previously noted trend of lower propellant stress relaxation modulus in the forward end of the motor and higher modulus in the barrel near the equators and under the grounding straps is still in evidence. This correlation suggests the relationship of bond strength to propellant relaxation modulus.

5.3.3 V-45 Insulation Material Properties

The relaxation modulus, moisture content, dioetylphthalate (DOP)
plasticizer content, and swell ratio of V-45 insulation were determined
in various locations of motor TC 30072. The V-45 relaxation modulus is
typically lowest in the equator region and highest in the forward and aft
flaps. The V-45 moisture content results show that the percent moisture
is lowest in the barrel region. The test results are summarized in Tables
44 to 48.

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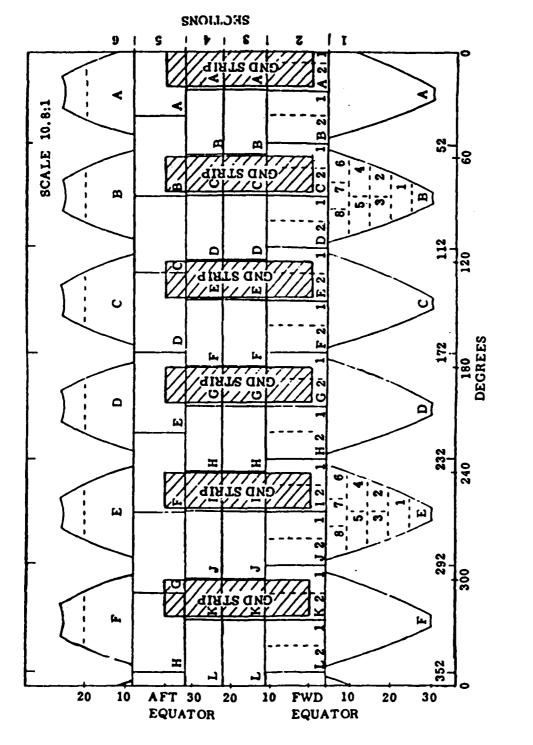


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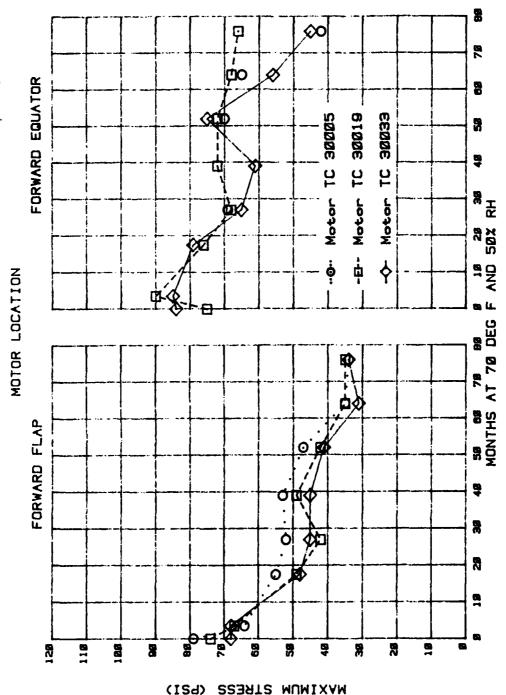
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Definition Flowchart for Minuteman Stage III Surveillance Program Figure 1.



igure 2. Motor Segment Layout





Effect of Storage Conditions Upon Mini DPT Bond Strength in the Forward Flap and at the Forward Equator Figure 3.

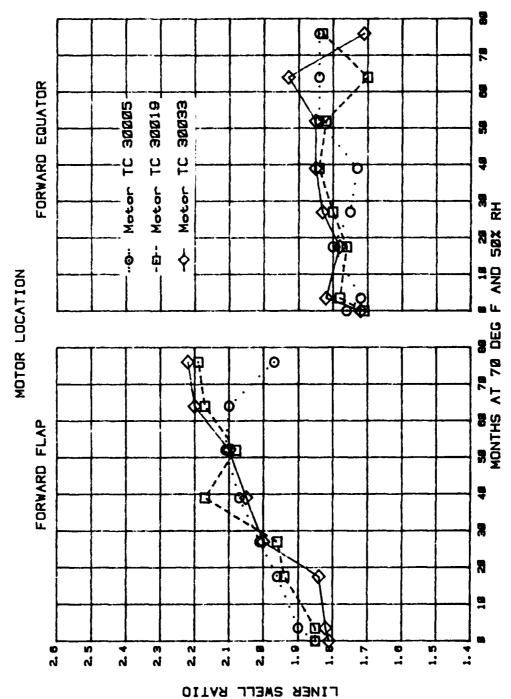
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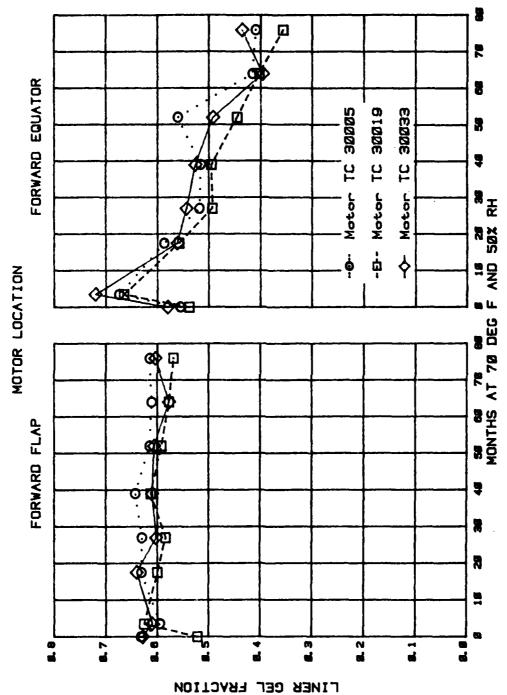
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Effect of Storage Conditions Upon Liner Swell Ratio at the Forward Flap and Forward Equator Figure 4.

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Effect of Storage Conditions Upon Liner Gel Fraction at the Forward Flap and at the Forward Equator Figure 5.

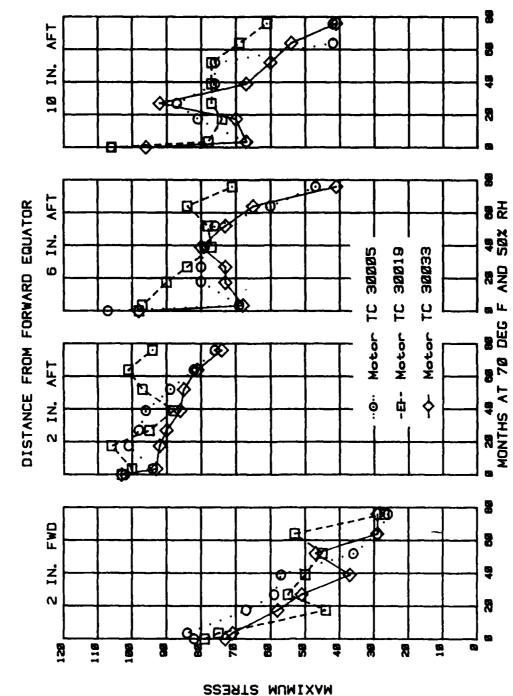
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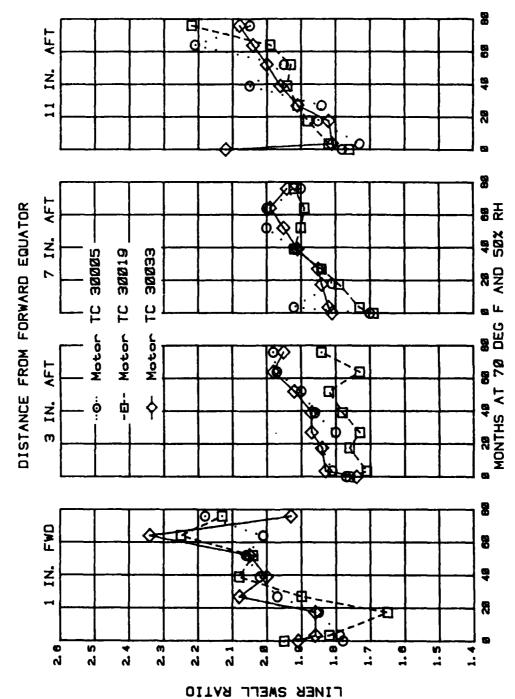


Effect of Storage Conditions Upon Mini DPT Bond Strength Near the Forward Equator Figure 6.

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Storage Conditions Upon Liner Swell Ratio Near the Forward Equator Effect of Figure 7.

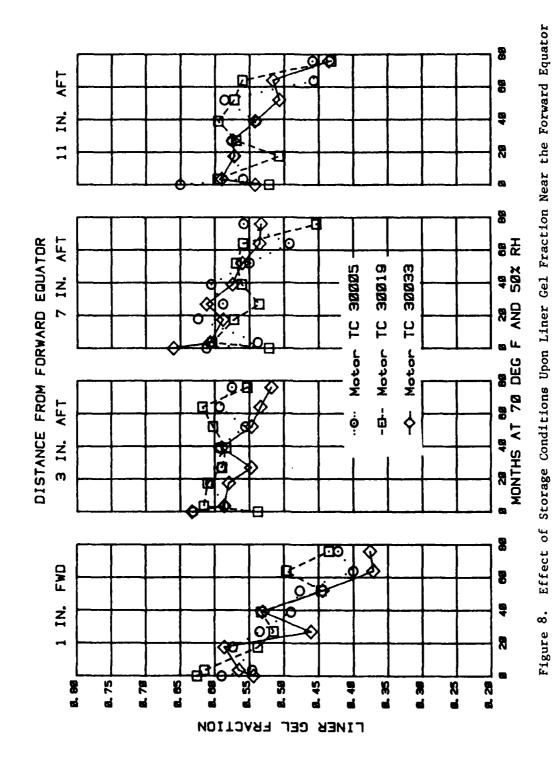
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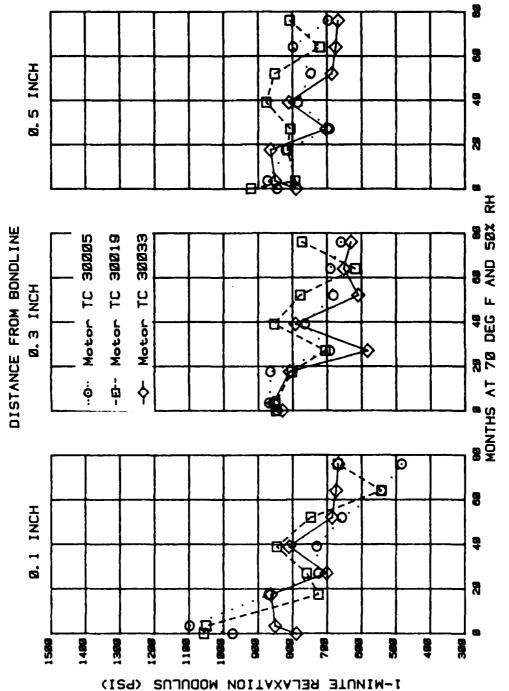


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Effect of Storage Conditions Upon Propellant Relaxation Modulus in the Forward Flap Area Figure 9.

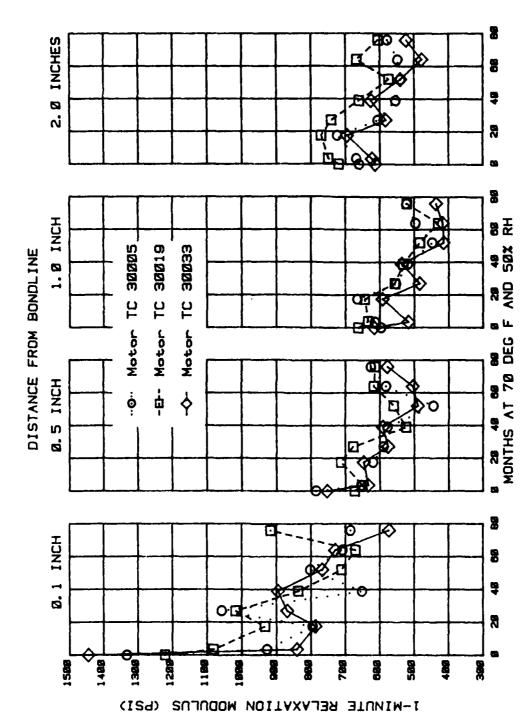
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Effect of Storage Conditions Upon Propellant Relaxation Modulus at the Forward Equator Figure 10.

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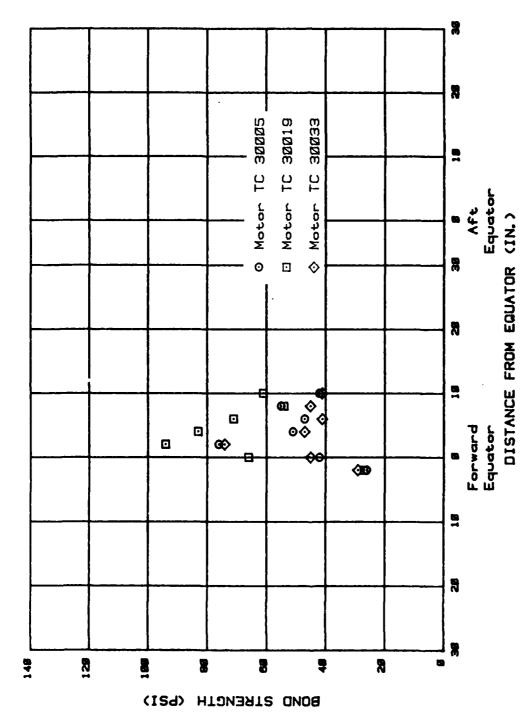


Figure 11. Mini DPT Bond Strength at Various Motor Locations

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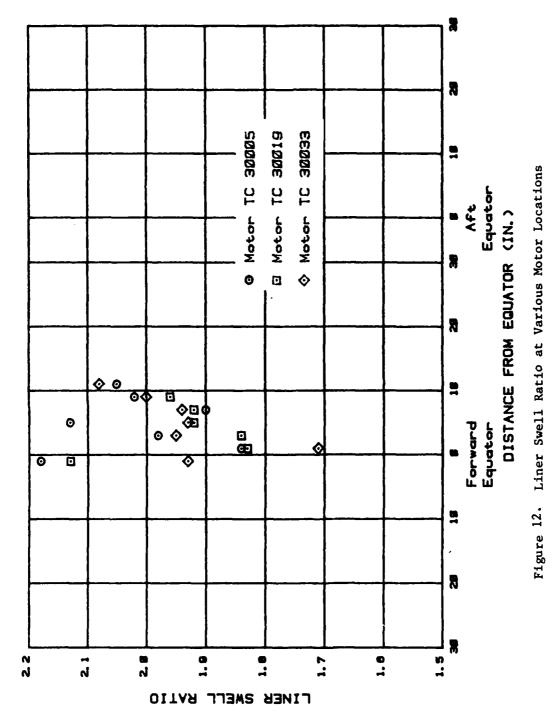
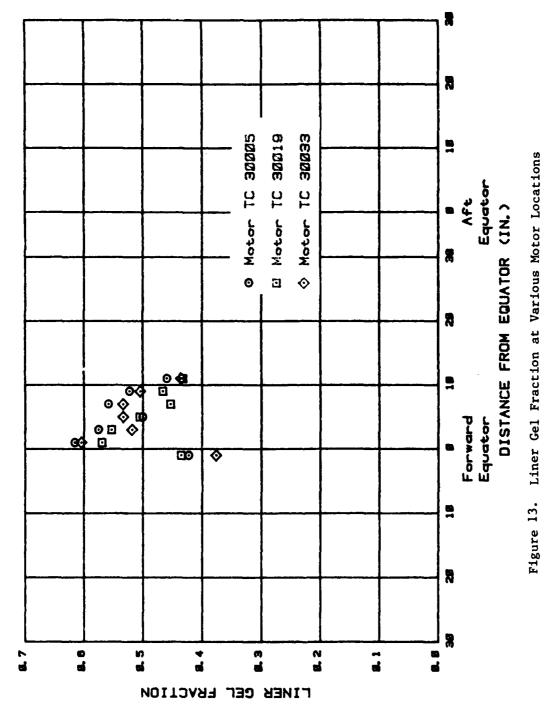


Figure 12. Liner Swell Ratio at Various Motor Locations

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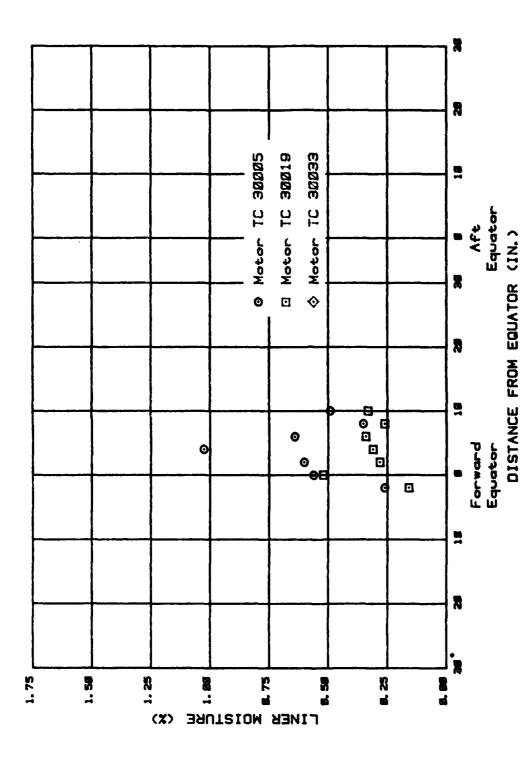
Liner Gel Fraction at Various Motor Locations Figure 13.

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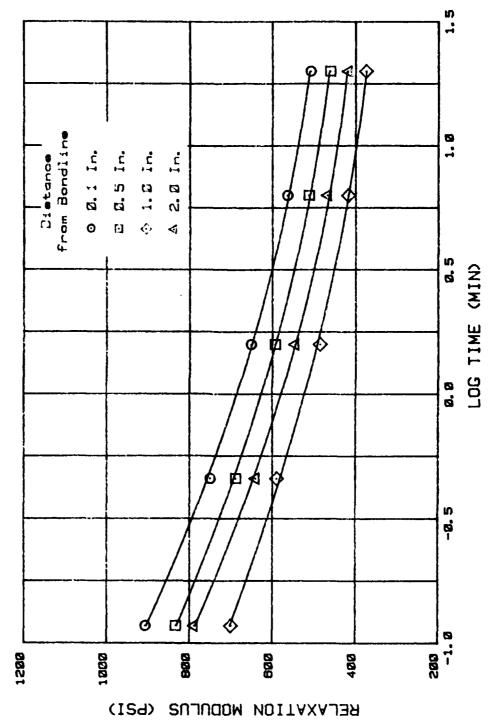
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Figure 14. Liner Moisture at Various Motor Locations

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Motor TC 30005 Relaxation Modulus of ANB-3066 Propellant at the Forward Equator Figure 15.

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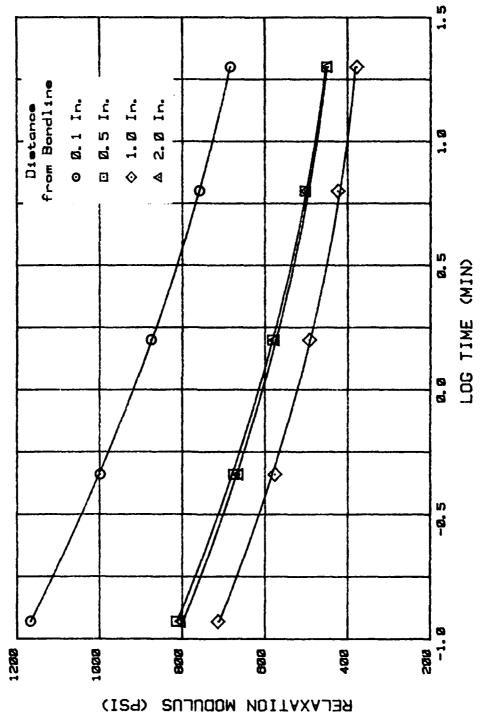
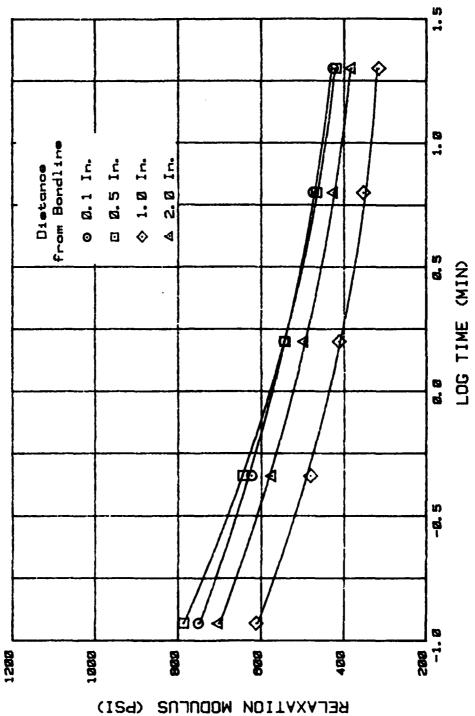


Figure 16. Motor TC 30019 Relaxation Modulus of ANB-3066 Propellant at the Forward Equator

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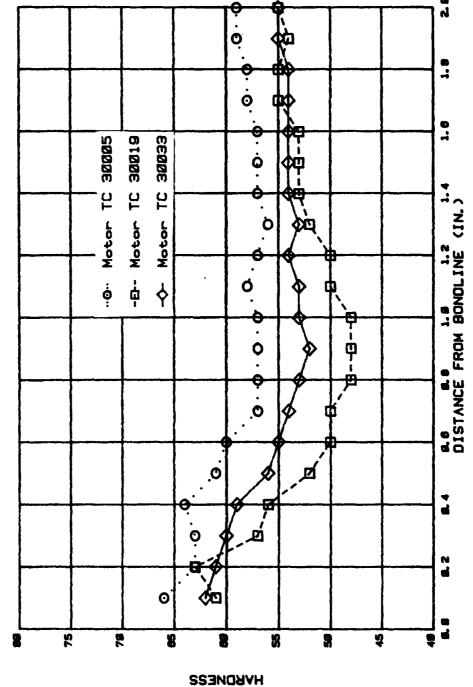
Motor TC 30033 Relaxation Modulus of ANB-3066 Propellant at the Forward Equator Figure 17.

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Figure 18. Shore A Hardness Gradient of ANB-3066 Propellant at the Forward Equator

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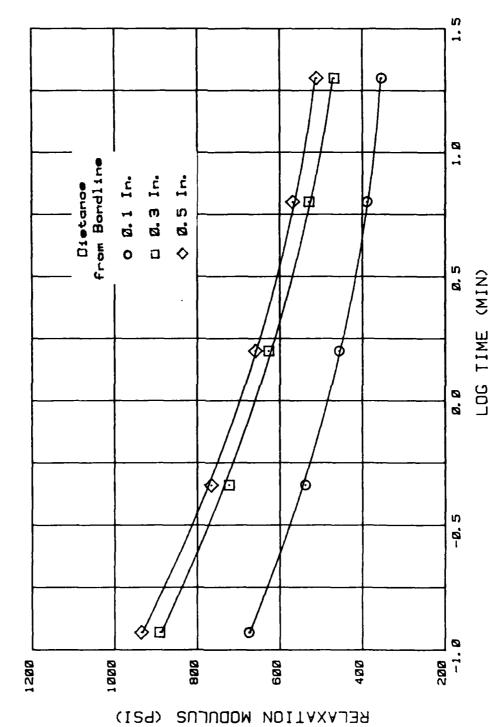
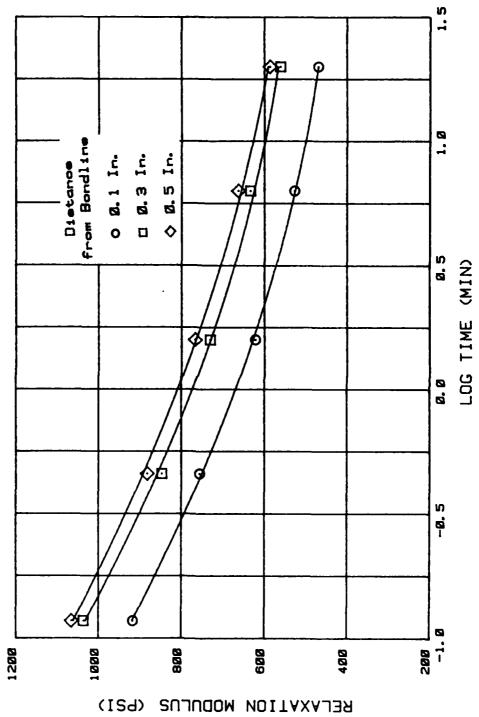


Figure 19. Notor TC 30005 Relaxation Modulus of ANB-3066 Propellant in the Forward Flap Area

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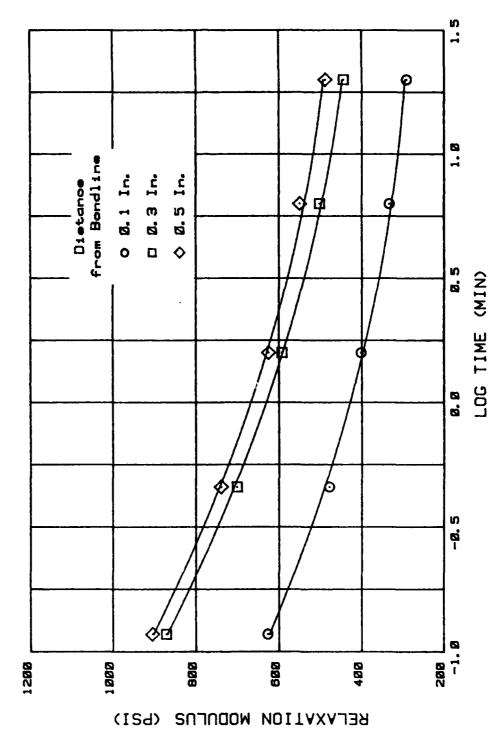


Motor TC 30019 Relaxation Modulus of ANB-3066 Propellant in the Forward Flap Area Figure 20.

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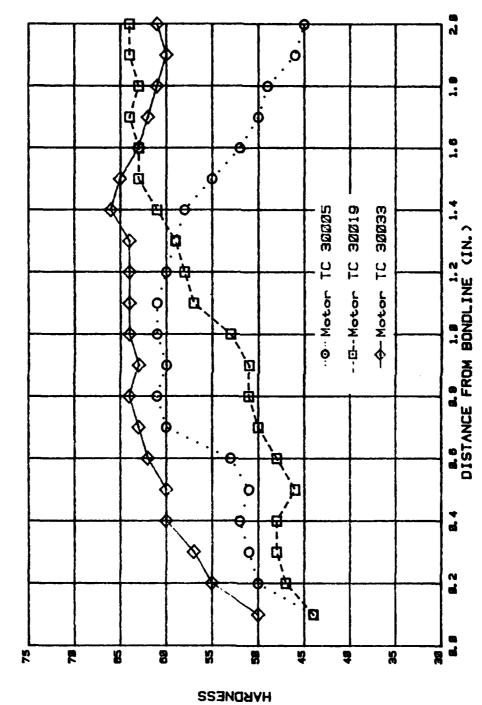
Motor TC 30033 Relaxation Modulus of ANB-3066 Propellant in the Forward Flap Area Figure 21.

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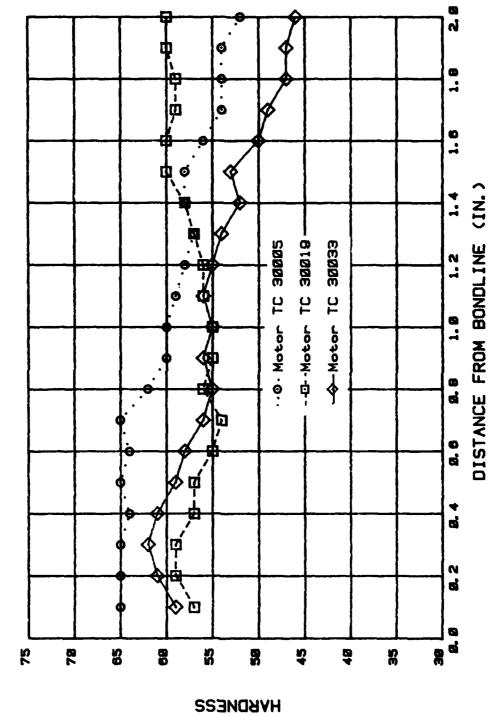
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Shore A Hardness Gradient of ANB-3066 Propellant in the Forward Flap, Area A Figure 22.

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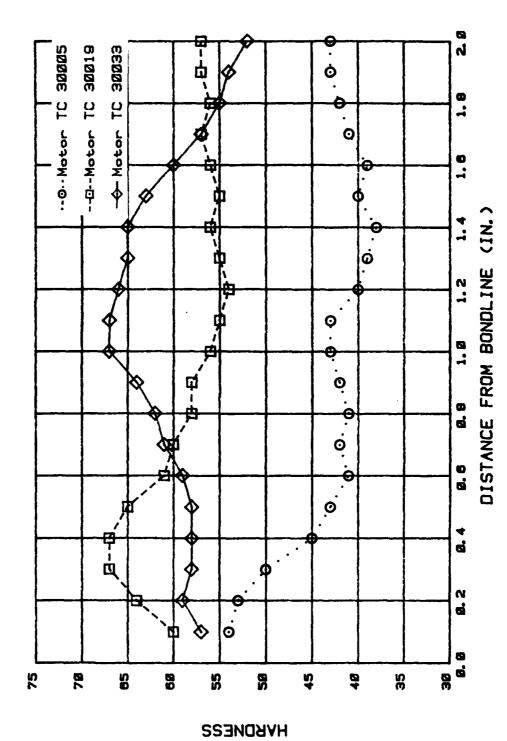
Shore A Hardness Gradient of ANB-3066 Propellant in the Forward Flap, Area B Figure 23.

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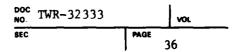
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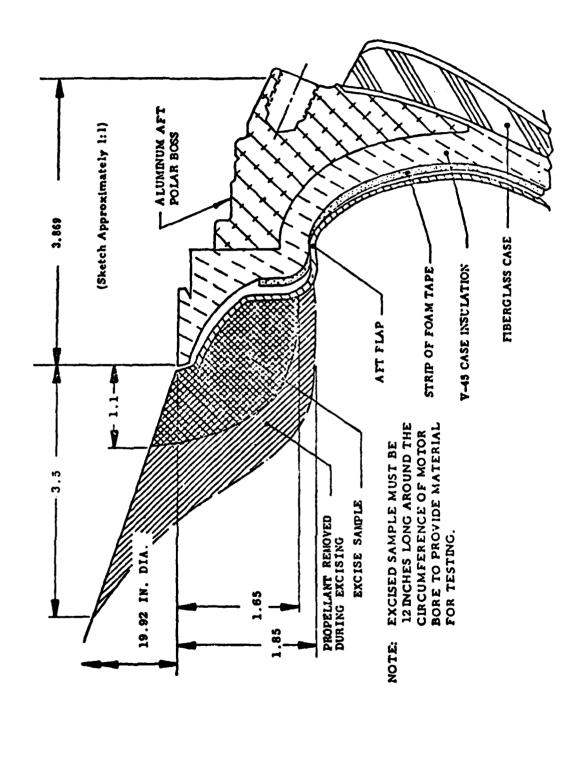
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Shore A Hardness Gradient of ANB-3066 Propellant in the Forward Flap, Area C Figure 24.

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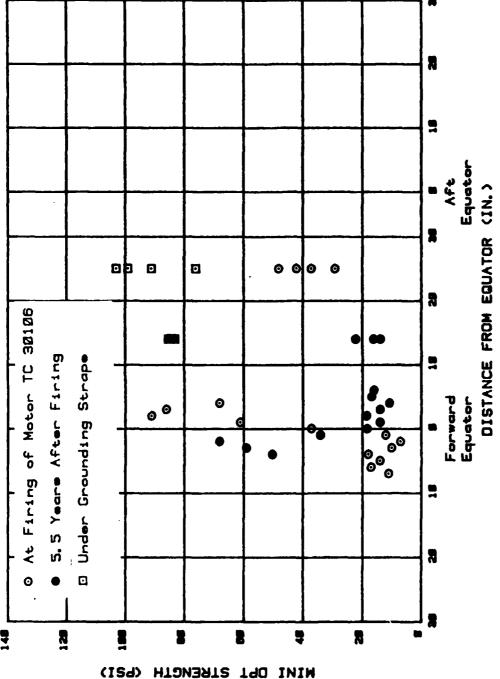
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Figure 25. Excixe Sample Diagram

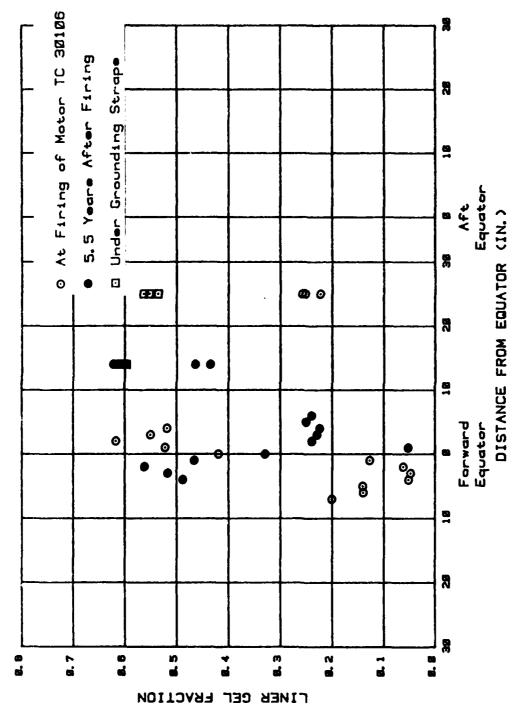


Liner Bond Tensile Strength at Various Motor Locations: Motor TC 30050 Segments at Time of Firing of Motor TC 30106 and 5.5 Years Later Figure 26.

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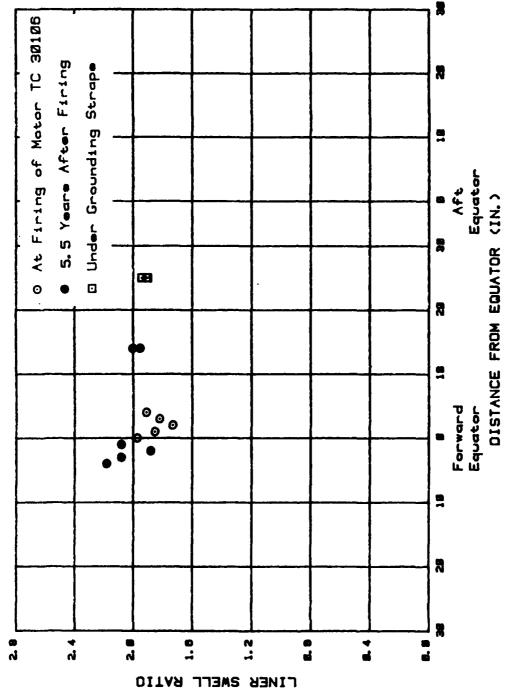
Motor TC 30050 Segments at Time of Firing of Motor TC 30106 and 5.5 Years Later Liner Gel Fraction at Various Motor Locations: Figure 27.

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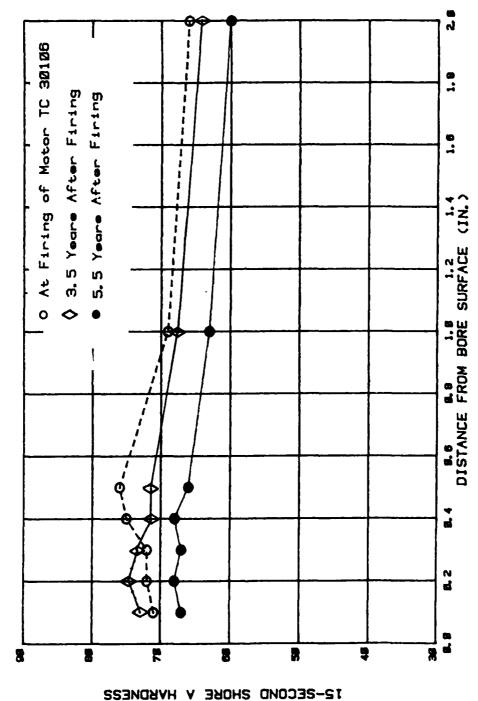


Liner Swell Ratio at Various Motor Locations: Motor TC 30050 Segments at Time of Firing of Motor TC 30106 and 5.5 Years Later Figure 28.

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Shore A Hardness of Bore Propellant: Motor TC 30050 Segments at Time of Firing of Motor TC 30106 and 5.5 Years Later Figure 29.

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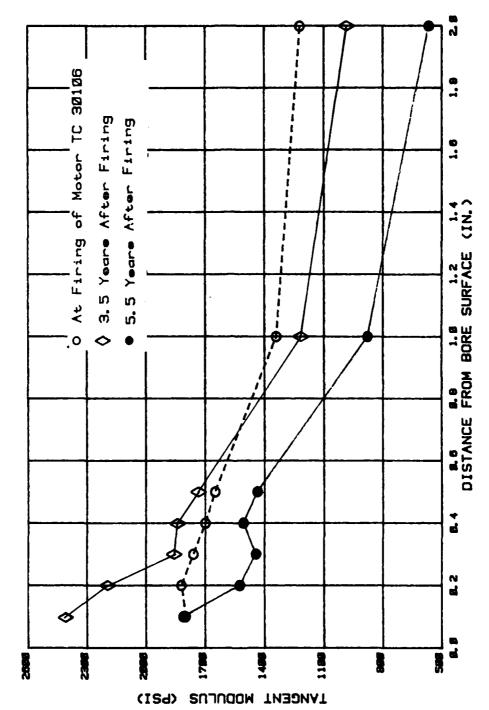
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Motor IC 30050 Segments Modulus of Mini Tensile Specimens from Bore Propellant: at Time of Firing of Motor TC 30106 and 5.5 Years Later Figure 30.

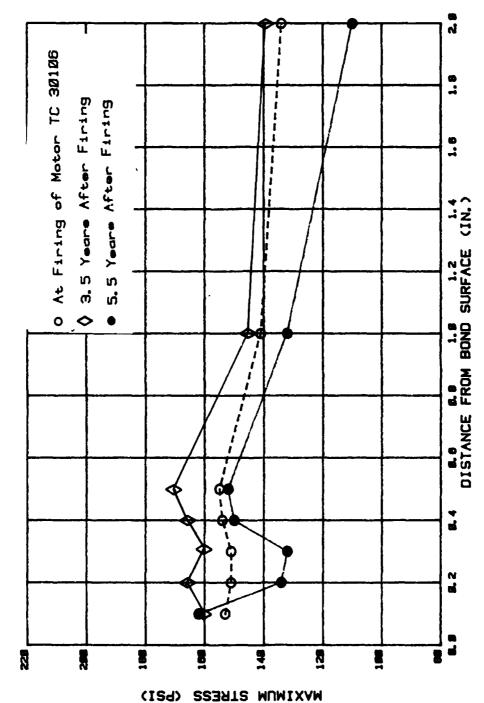
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Maximum Stress of Mini Tensile Specimens from Bore Propellant: Motor TC 30050 Segments at Time of Firing of Motor TC 30106, 3.5 and 5.5 Years Later Figure 31.

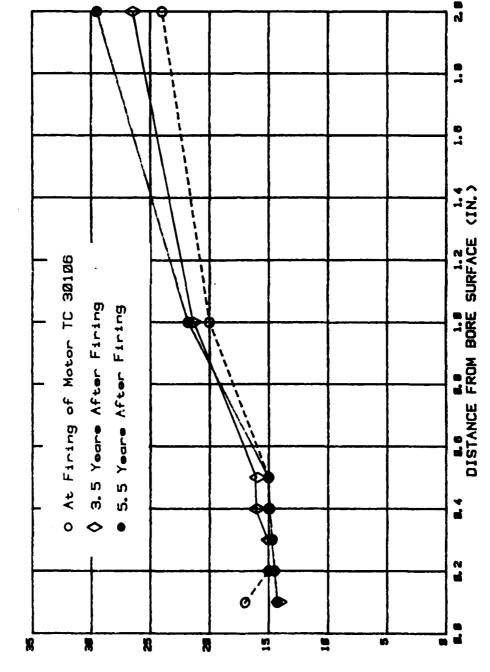
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Strain at Maximum Stress of Mini Tensile Specimens from Bore Propellant: Motor TC 30050 Segments at Time of Firing of Motor TC 30106, 3.5 and 5.5 Years Later Figure 32.

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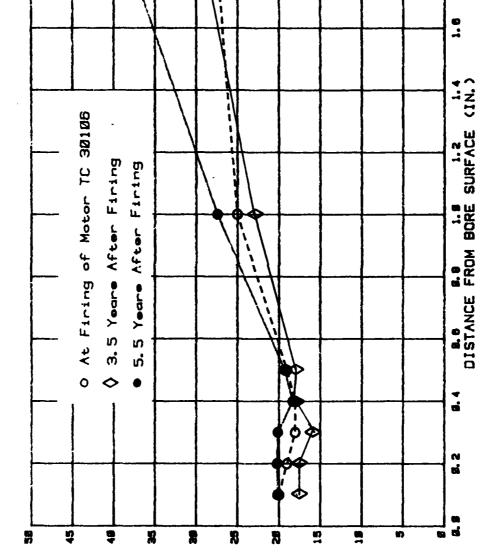
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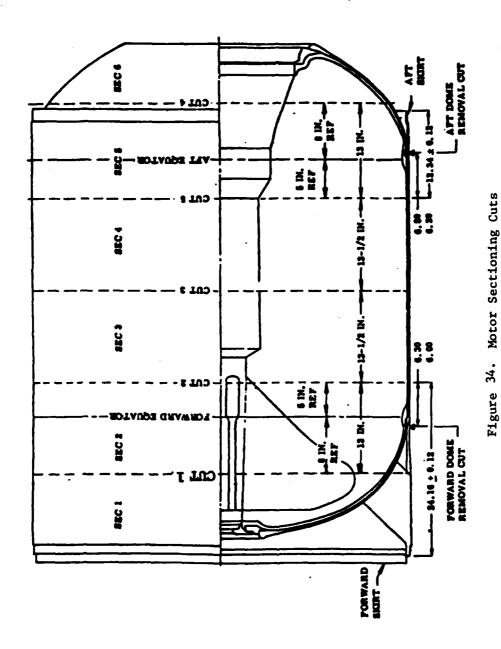
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Strain at Failure of Mini Tensile Specimens from Bore Propellant: Motor TC 30050 Segments at Time of Firing of Motor TC 30106, 3.5 and 5.5 Years Later Figure 33.



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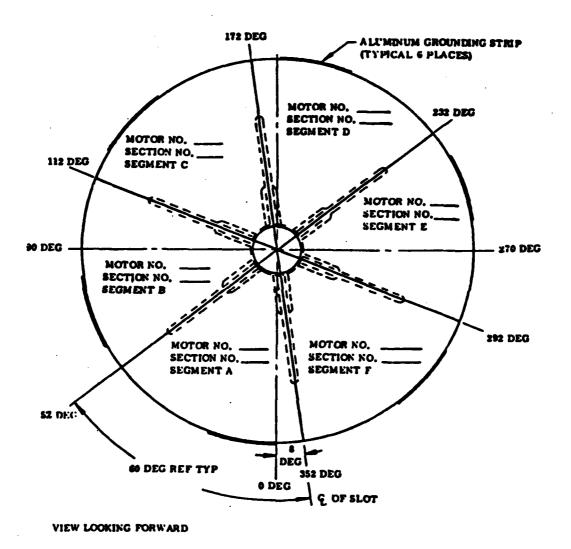


Figure 35. Segment Cuts for Section 1

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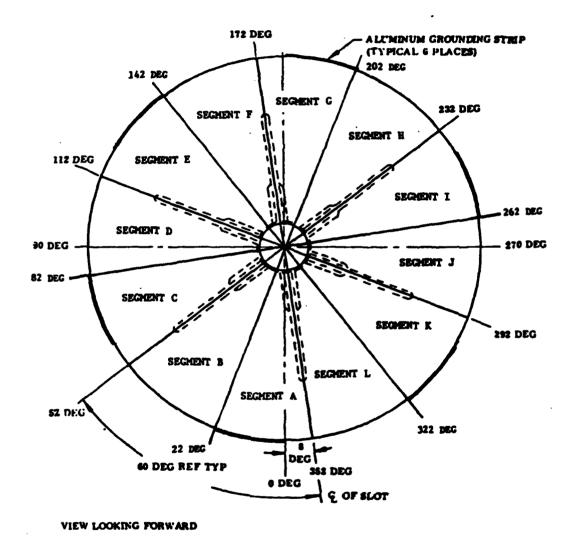
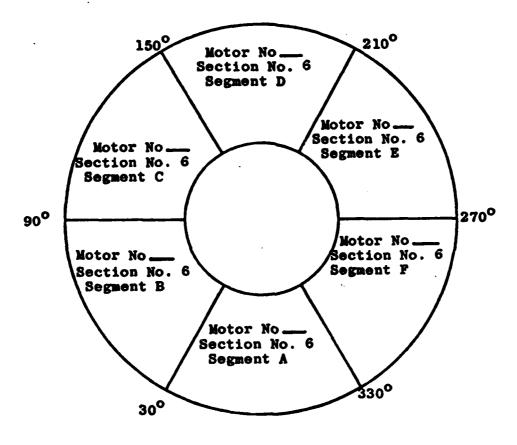


Figure 36. Segment Cuts for Section 2

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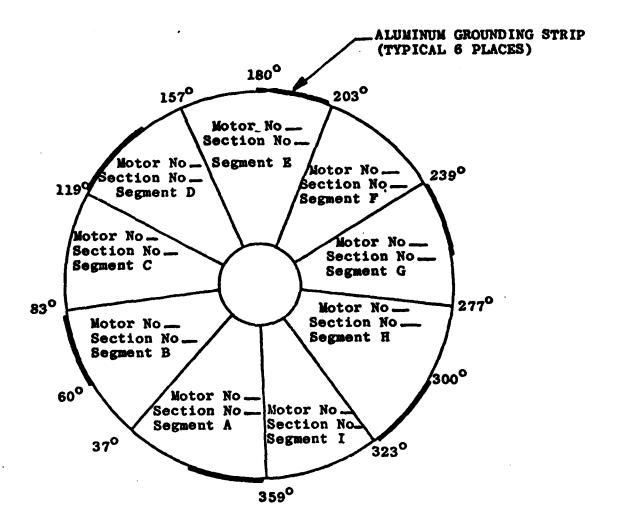


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Figure 37. Segment Cuts for Sections 3, 4, and 5

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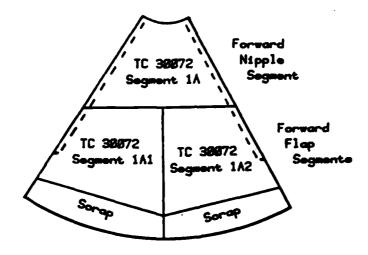


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Figure 38. Segment Cuts for Section 6

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Figure 39. Additional Cutting and Typical Marking of Section 1 Segments

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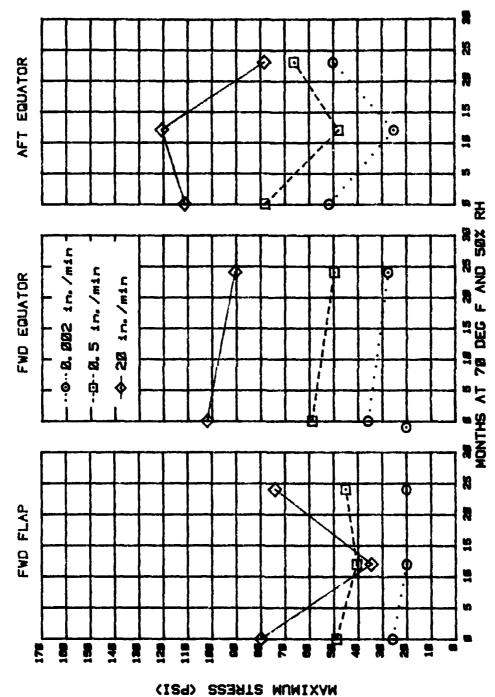
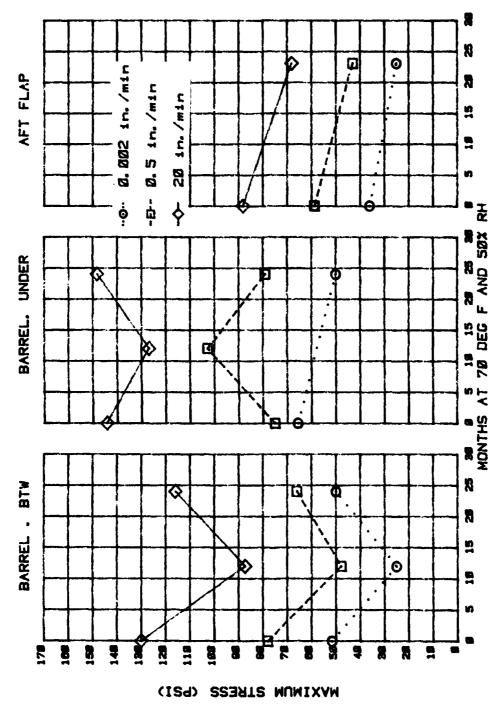


Figure 40. Mini DPT Bond Strength in Motor TC 30072 at Various Motor Locations

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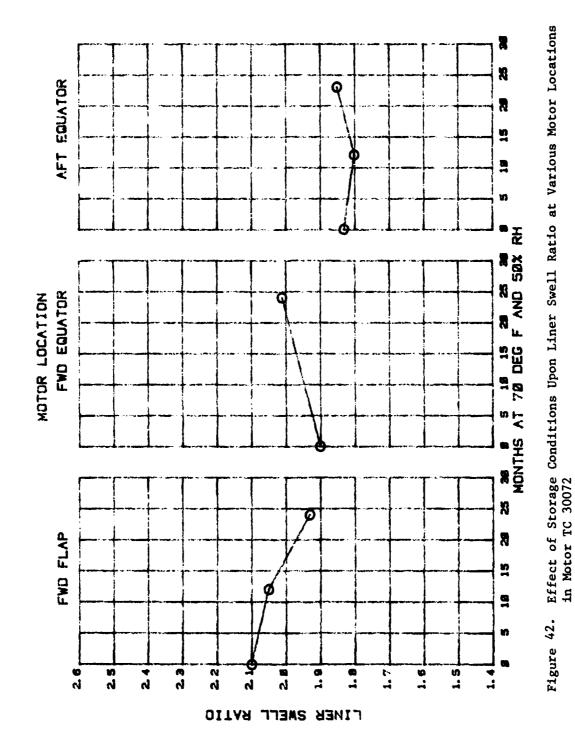


Mini DPT Bond Strength in Motor TC 30072 at Various Motor Locations Figure 41.

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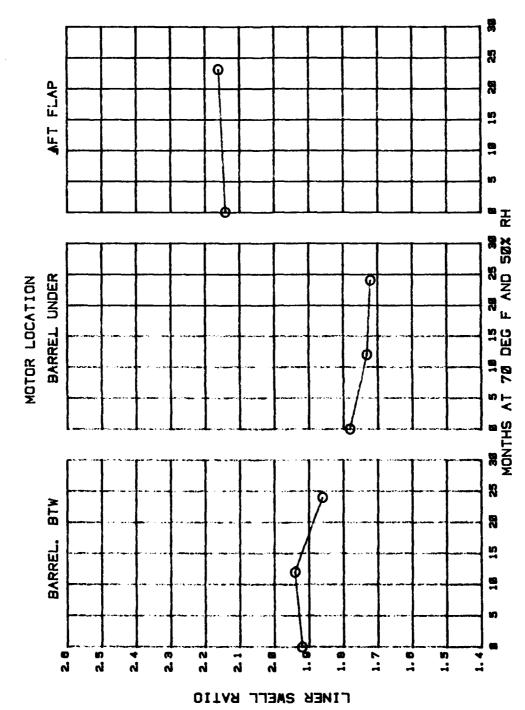
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Effect of Storage Conditions Upon Liner Swell Ratio at Various Motor Locations in Motor TC 30072Figure 43.

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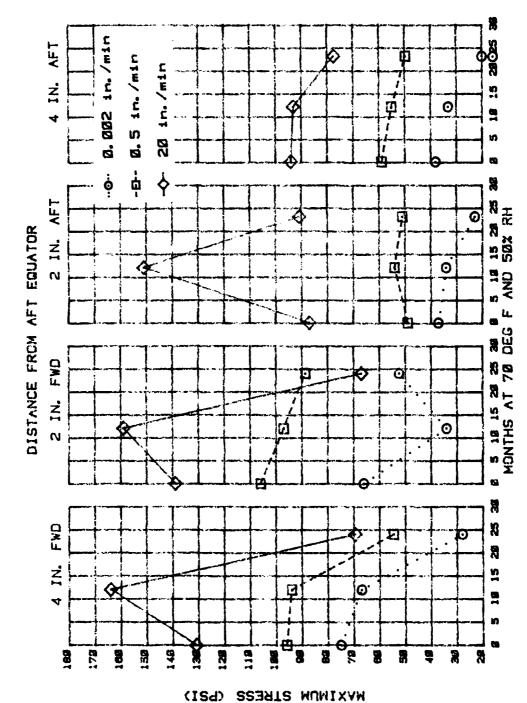
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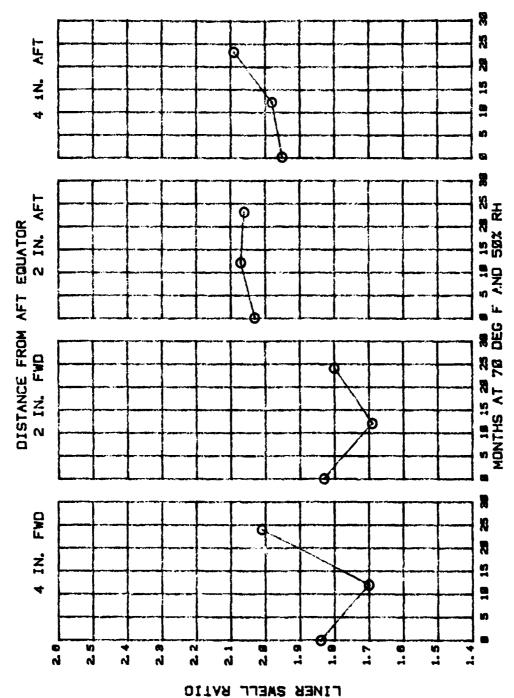


Effect of Storage Conditions Upon Mini DPT Bond Strength Near the Aft Equator of Motor TC 30072Figure 44.

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Effect of Storage Conditions Upon Liner Swell Ratio Near the Aft Equator of Motor IC 30072Figure 45.

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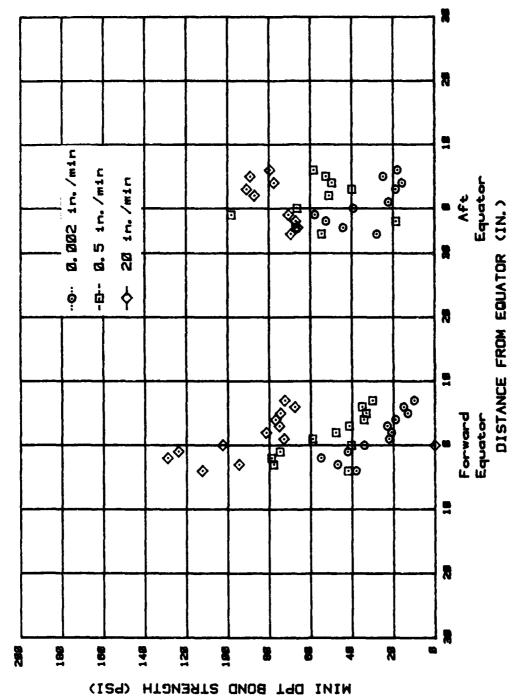


Figure 46. Mini DPT Bond Strength at Various Motor Locations in Motor TC 30072

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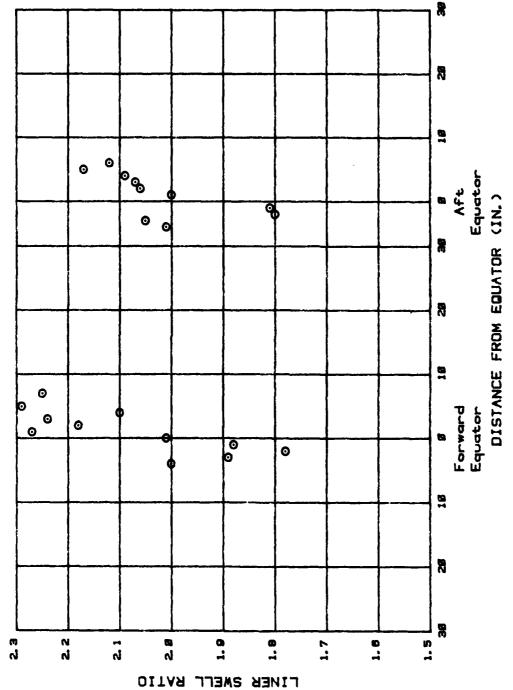
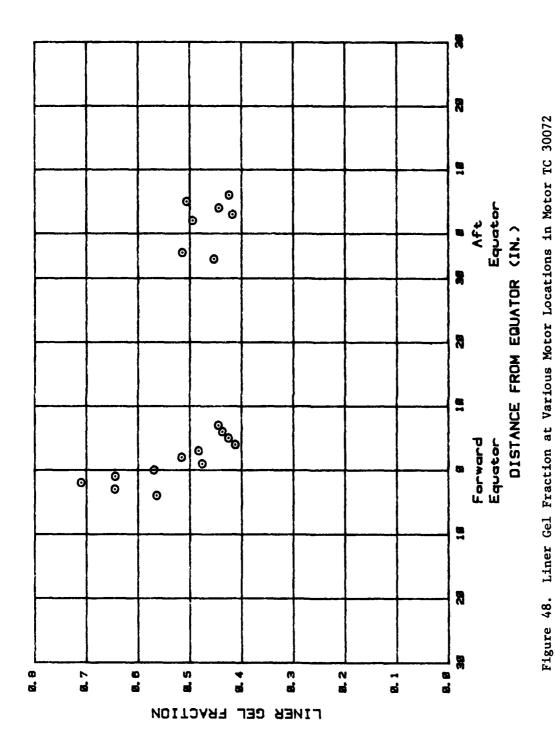


Figure 47. Liner Swell Ratio at Various Motor Locations in Motor TC 30072

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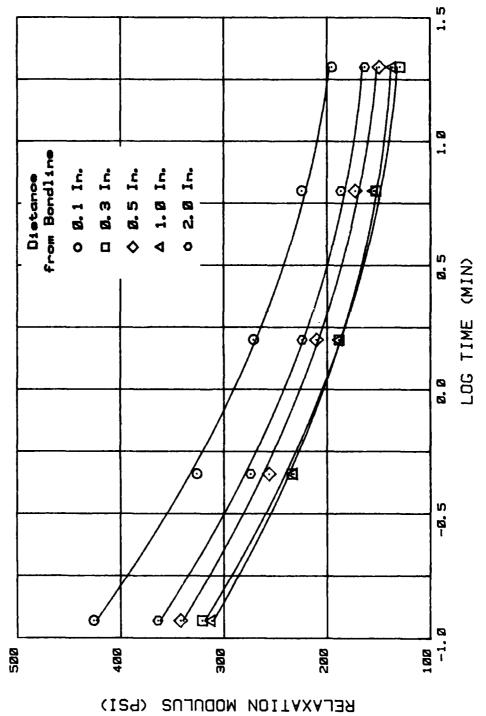
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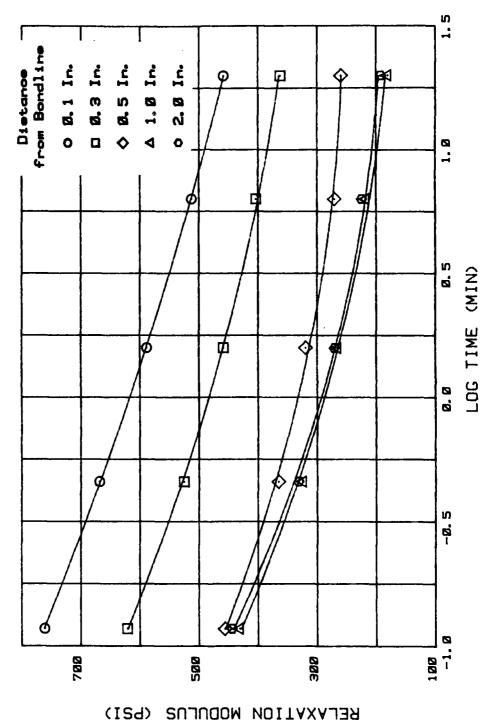


Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Forward Flap, Segment 1Al Figure 49.

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Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant in the Barrel Area, Under the Grounding Straps Figure 50.

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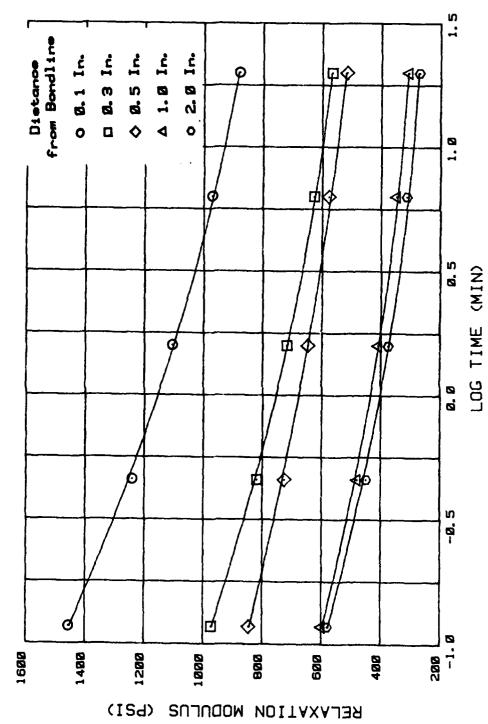
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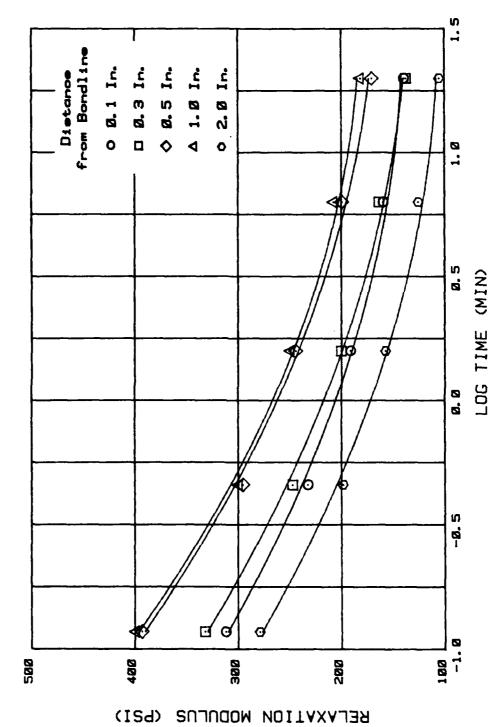


Notor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant in the Barrel, Under Grounding Straps Figure 51.

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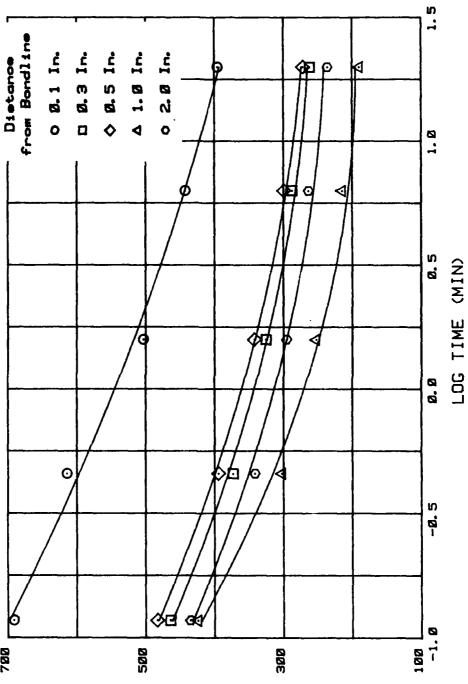
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Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Forward Nipple Area Figure 52.

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RELAXATION MODULUS (PSI)

Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Forward Equator, Area A Figure 53.

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from Bondline 2; 8 0 13.1 LOG TIME (MIN) 700 500 300

RELAXATION MODULUS (PSI)

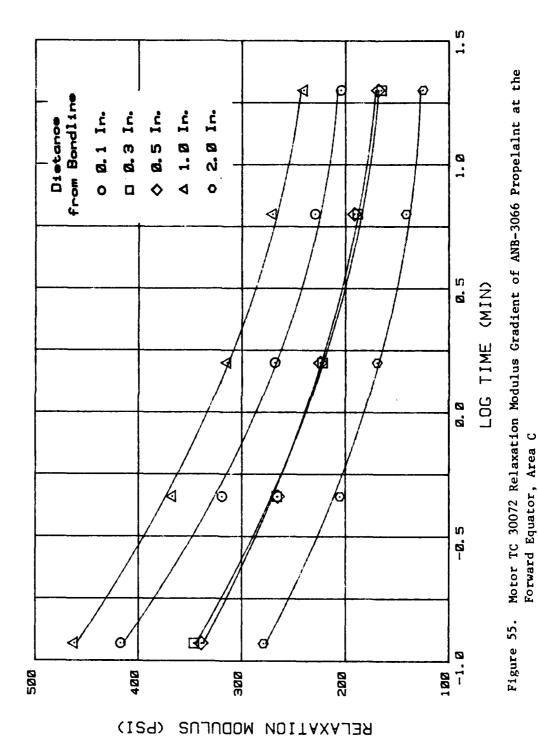
Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Forward Equator, Area B Figure 54.

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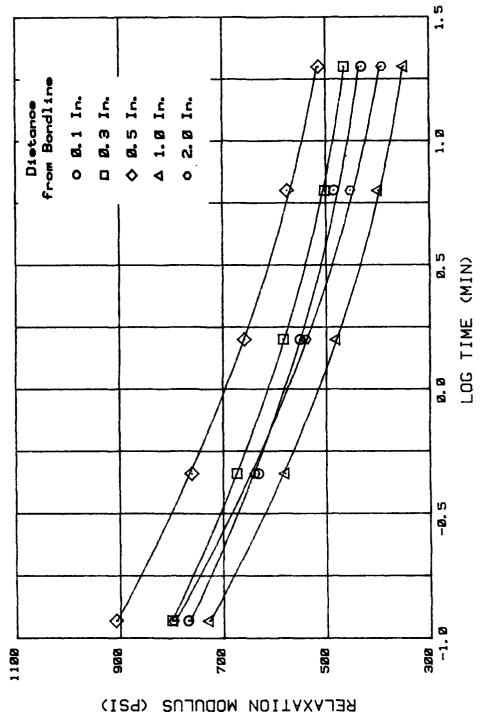
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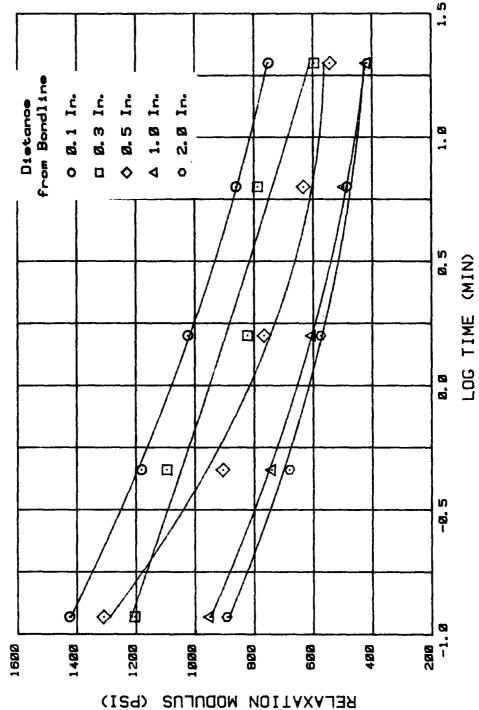
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Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Aft Equator, Area A Figure 56.

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Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Aft Equator, Area B Figure 57.

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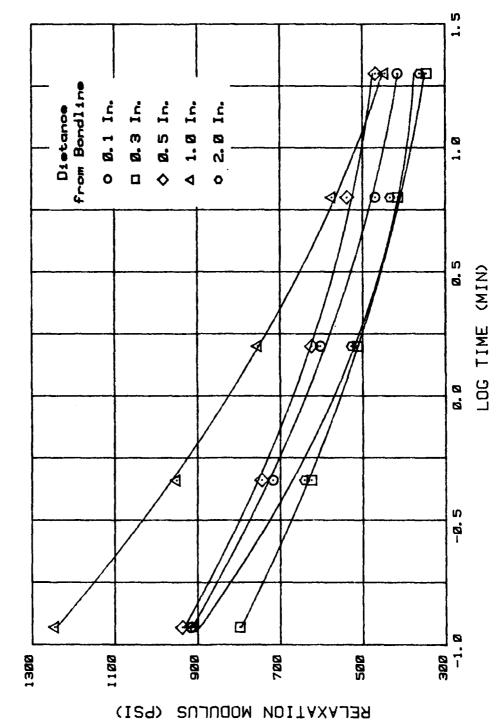
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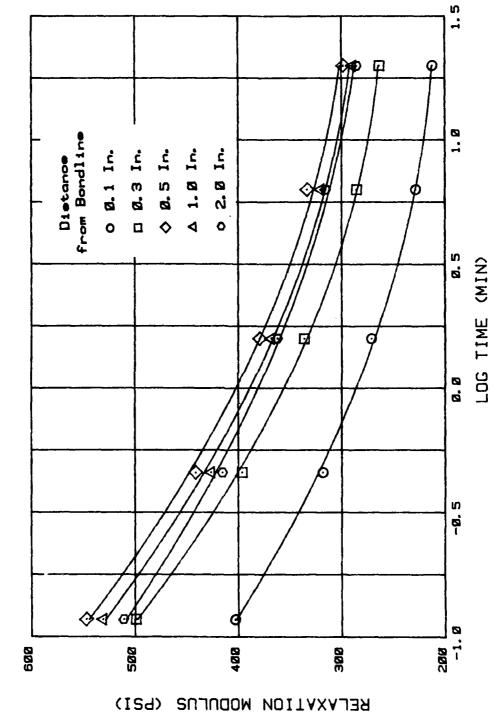


Notor TC 30072 Relaxation Gradient of ANB-3066 Propellant at the Aft Equator, Area C Figure 58.

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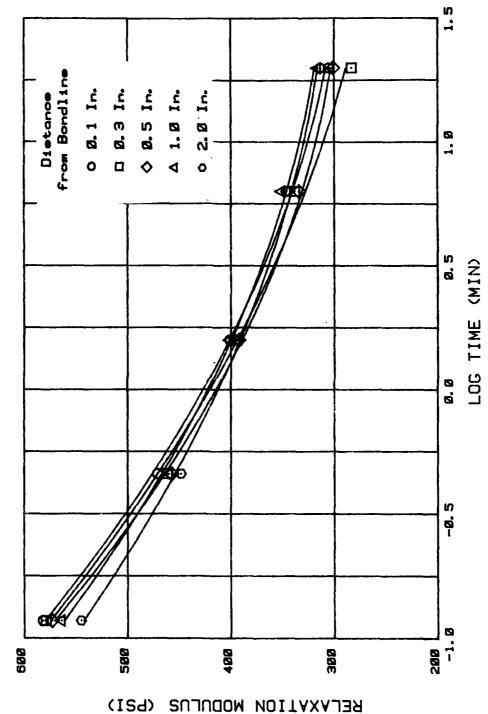


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Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Aft Flap, Area D Figure 59.

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Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Aft Flap, Area E Figure 60.

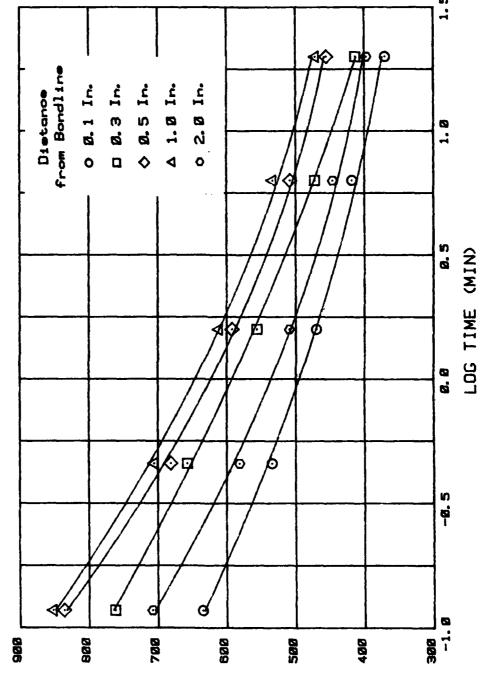
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RELAXATION MODULUS (PSI)

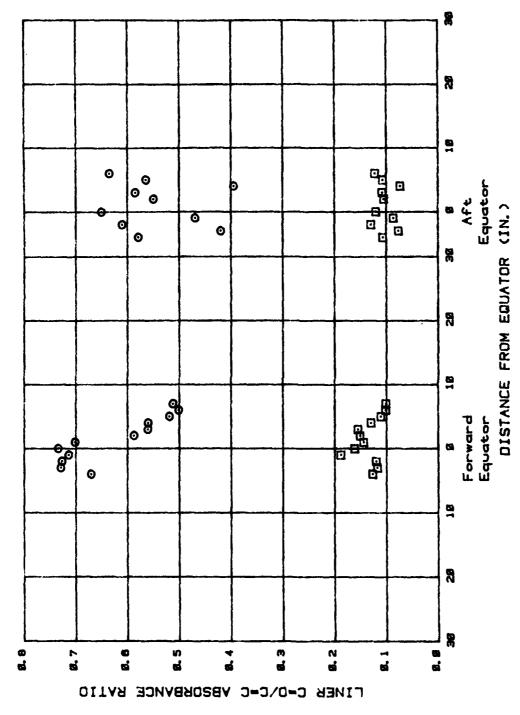
Motor TC 30072 Relaxation Modulus Gradient of ANB-3066 Propellant at the Aft Flap, Area F Figure 61.

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Motor TC 30072 Liner C=0/C=C (Vinyl and Stretching) Absorbance Ratio at Various Motor Locations Figure 62.

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TABLE 1

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SECHENT USAGE BY TEST DATE

		Identification	Identification of Motor Segments*	*81	
Test Date	Berrel, Between Aluminum Straps	Barrel, Under Aluminum Straps	Forward Equator	Aft Flap Near Bore	Flap
1978	3D, 4D	30, 40	201	89	181
1979	3H**	36	2H1	None	125
1980	31	3K	21.1	None	138
1961	None	None	201		183
1982	43	14	231	None	126
1983	None	None	281	None	184
1984	45	H 7	27.1	ပ္	123
1985	None	None	21.2	None	186
1986	75	4K	202	None	128
1987	None	None	232	67	182
1988	38	*	. 282	None	154
1989	None	None	27.2	None	185
1990	Н7	94	2H2	9	121
Spare	3P**, 3J, 4B	3E, 31, 4A	2A1, 2E1, 2G1, 2I1, 2K1	\$	187, 1E2, 1E7
	1				

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TABLE 2

Server Conservation Conservation

MATRIX FOR MINITERAN STAGE III BONDLINE AGING PROGRAM

Number/ Notor	•	•	m	22	ოოოო	•	๓๓๓๓
Specimen	Poker Chip	Round Flap	Mini-DPT	Mini-Tensile (Shore A)	Penetrometer	Poker Chip	Penetrometer
Test Conditions (1)	Constant Strain Rate	Constant Strain Rate	0,5 in/min	2.0% Strain 15 sec.	10 sec.	Constant Strain Rate	10 sec.
Haterial Property	Bond Shear	Bond Tensile(2)	Bond Tensile	En Profile (3) Hardness (4)	ER Swell Ratio Gel Fraction Moisture	Bond Shear	PR Swell Ratio Gel Fraction Moisture
Materiels	ANB-3066/ SD-851-2/V-45			ANB-3066	\$D-851-2	ANB-3066/ SD-851-2/v-45	SD-851-2
Sample Area	Barrel, Between Aluminum Straps					Barrel, Under Aluminum Straps	

(1)All tests at 77°F, 0 psi.

(2)See text, Sections 4.2.1.1 and 4.2.1.2. (3)0.1, 0.5, 1.0, and 2.0 in. from bondline.

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TABLE 2 (CONT)

D

MATRIX FOR MINITERAN STACE III BONDLING ACING PROGRAM

Sample Area	Materials	Material Property	Test (1)	Specimen	Member/ Motor
Forvard Equator	ANB-3066/ SD-851-2/V-45	Bond Tensile Profile (5)	0.5 in./aia.	Mint-DFT	21
	ANB-3066	E _R Gradient (6) Hardness (4)	2.0% Strain 15 Sec.	Mini-Tensile (Shore A)	22
	\$D-851-2	ER (S) Swell Ratio (S) Gel Fraction (S) Moisture (S)	10 sec.	Penetrometer	2222
Aft Flap Hear bore area (7)	ANB-3066/ SD-851-2/V-45	Bond Tensile (B)	0.5 in./sin.	Mat-DFT	•
	ANB-3066	ER Gradient (9)	2.0% Strain	Mini-Tensile	•
	SD-851-2	Svell Ratio (8)	; ; ; ;	(v 370m)	1 A Ø
	A-45	Moisture			• • •
		Margness Er	2.0% Strain	(Shore A) 0.05 x 0.5 x 4	1 M
		DOP Content	:	:	n (
		Swell Ratio	:	:	•

Forward Flap Testing will be identical to aft flap.

(S)2 in. forward to 10 in. aft of forward equator in 2 in. increments, 7 locations (between aluminum

(6) 11, 0.5, 1.0, and 2.0 in. from bondline at equator only.

(7) Sample at 3 year intervals.

(9) Taken from 3 separate locations along the sample.
(9) Test at 0.1, 0.3, and 0.5 in. from bond interface.

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TABLE 3

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MOTOR TC 30005 MATERIAL PROPERTIES DATA FORWARD EQUATOR AREA, SEGMENT 2L2

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						SEC		PAGE 7.8	
/ISION	_					DOC NO. TWR	-32333	VOL	
	Distance Aft of Forward	Equator (in.)	-2	0	2	4	9	ω	10
	Maximum Stress	(psi)	22 24 33 26	45 43 43	74 82 72 76	61 48 51	48 34 47	60 58 47 55	34 53 43
	Failu	APL	សសស	70 27	75 80 80	80 80	09 07 07	80 80 80	09
7	Failure Mode (%)	티	95 95 95	30	25 20 20	20 20 20	50 50 40	20 20 20	07 07 07
7-YEAR	(%)	CF1	1 1 1	i 1	1 1 1	1 1 1	10	1 1 3	1 1 1
7-YEAR (1985) RESULTS	Liner Moisture	(%)	0.26	0.56	09.0	1.02	0.64	0.35	0.49
	Distance Aft of Forward	Equator (in.)	7		က	'n	7	6	11
	Liner Swell	Ratio	2.20 2.13 2.20 2.18	1.84 1.85 1.83 1.84	1.94 2.00 2.00 1.98	$\begin{array}{c} 2.16 \\ 2.13 \\ \hline 2.09 \\ \hline 2.13 \end{array}$	$\begin{array}{c} 1.88 \\ 1.88 \\ \hline 1.93 \\ \hline 1.90 \end{array}$	2.06 2.00 2.00 2.02	$\begin{array}{c} 2.07 \\ 2.00 \\ \hline 2.07 \\ \hline 2.05 \end{array}$
	Liner Gel	Fraction	0.395 0.431 0.440 0.422	0.626 0.609 0.610 0.615	0.565 0.593 0.566 0.575	0.508 0.502 0.490 0.500	$\begin{array}{c} 0.585 \\ 0.577 \\ 0.511 \\ \hline 0.558 \end{array}$	$\begin{array}{c} 0.513 \\ 0.518 \\ 0.534 \\ \hline 0.522 \end{array}$	0.463 0.480 0.432 0.459

TABLE 4

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MOTOR TC 30019 MATERIAL PROPERTIES DATA FORWARD EQUATOR AREA, SEGMENT 2L2 7-YFAR (1985) RESHITS

					SEC		PAGE 70	
BION	_				DOC NO. TWR	-32333	VOL	
	Distance Aft of Forward Equator (in.)	-2	0	2	4	9	∞	10
	Maximum Stress (psi)	30 24 27	66 66 66 66 66	94 90 97	83 83 83	63 80 71 71	52 45 <u>64</u> 54	57 77 50 61
	Failt	i i	75 90 80	80 80 80	95 95 90	95 95 95	80 70 80	80 80 80
	Failure Mode (%) APL CL CLI	100 100 95	25 10 20	20 20 20	5 20	יט יט יט	20 20 20	20 20 20
7-year	(%) CLI	1 1	1 1 1	1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
7-year (1985) results	Liner Moisture (%)	0.16	0.52	0.28	0.31	0.34	0.26	0.33
	Distance Aft of Forward Equator (in.)	-1	г	m	'n	7	o s	п
	Liner Swell Ratio	2.11 2.17 2.11 2.13	1.83 1.89 1.78 1.83	1.86 1.83 1.83	2.00 1.88 1.88	1.92 1.92 1.92 1.92	1.87 2.00 2.00 1.96	2.24 2.24 2.19 2.22
	Liner Gel Fraction	0.449 0.426 0.430 0.435	0.577 0.568 0.561 0.561	0.573 0.536 0.554 0.553	$\begin{array}{c} 0.524 \\ 0.510 \\ 0.483 \\ 0.505 \end{array}$	0.457 0.444 0.453	0.462 0.443 0.494 0.466	0.441 0.423 0.432

TABLE 5

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MOTOR TC 30033 MATERIAL PROPERTIES DATA FORWARD EQUATOR AREA, SEGMENT 2L2 7-YEAR (1985) RESULTS

				SEC	· <u>-</u> · · · · · · · · · · · · · · · · · · ·	PAGE 80	"
<u>-</u>				DOC NO. TWI	R-32333	VOL	
Distance Aft of Forward Equator (in.)	-2	0	2	4	vo	0 0	10
Maximum Stress (psi)	36 29 19 29	41 47 47 45	77 77 69 74	42 40 59 47	33 39 51 41	59 41 45	37 45 -
Failu	10	60 90 70	95 95 95	95 80 80	90 90 95	90 95 95	06
Failure Mode (%) APL CL CLI	90 100 100	40 30	ភេសស	20 20	10 10 5	10 5	10
(%)	1 1 1	1 1 1	1 1 1	1 ((1 1 1	1 1 1	1-1-1
Liner Moisture (%)	1	ı	ı	i	1	1	1
Distance Aft of Forward Equator (in.)	-1	т	ĸ	'n	7	σ	11
Liner Swell Ratio	1.91 1.95 1.93	1.78 1.65 1.70 1.71	1.93 2.00 1.93 1.95	1.93 1.93 1.93	1.93 1.93 1.97 1.94	2.00 2.00 2.00 2.00	2.06 2.13 2.06 2.08
Liner Gel Fraction	0.416 0.374 0.339 0.376	0.582 0.615 0.614 0.605	$\begin{array}{c} 0.525 \\ 0.513 \\ \hline 0.517 \\ \hline 0.518 \end{array}$	0.524 0.549 0.527	0.535 0.540 0.524 0.533	0.485 0.511 0.517 0.504	0.455 0.468 0.381 0.435

TABLE 6

Server and the server

MOTOR TC 30005 STRESS RELAXATION GRADIENT ANB-3066 PROPELLANT, FORWARD EQUATOR AREA, AMBIENT SEGMENT 2L2 7-YEAR (1985) RESULTS

1.30	398	477	387	377
	455	446	357	417
	672	-	378	459
	508	-	374	417
(ps1)	441	528	429	419
	502	496	398	470
	746	-	423	512
	563	512	417	467
Relaxation Modulus (psi) Log Time (min) -0.34 0.20 0.80	518	615	507	488
	579	571	453	551
	857	-	496	596
	651	593	485	545
Relaxatio Log	607 666 978 750	714 662 - 688	663 519 584 589	577 644 698 640
-0.93	753	867	742	716
	808	801	636	795
	1160	-	722	<u>856</u>
	907	834	700	789
Strain (%)	2.00	$\frac{1.99}{2.00}$	2.01 2.00 2.00 2.00	2.01 1.99 1.99 2.00
Time From Cutting (hrs)	2.3 3.0 3.1	2.9 3.1	3.1 3.1	2.5 3.6 3.6
Distance From Bondline (in.)	0.1	0.5	1.0	2.0

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TABLE 7

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MOTOR TC 30019 STRESS RELAXATION GRADIENT ANB-3066 PROPELLANT, FORWARD EQUATOR AREA, AMBIENT SEGMENT 2L2 7-YEAR (1985) RESULTS

1.30	606	567	357	394
	720	446	387	494
	723	338	387	451
	683	450	377	446
(ps1)	667	633	401	442
	803	498	435	552
	805	378	433	503
	758	503	423	499
elaxation Modulus Log Time (min	771	727	472	512
	924	576	504	633
	930	441	501	578
	875	581	492	574
Relaxation Modulus (ps1) Log Time (min) -0.34 0.20 0.80	884	851	557	594
	1050	663	583	728
	1060	511	585	662
	998	675	575	661
-0.93	1000	1000	699	729
	1250	808	720	879
	1250	635	721	794
	1167	814	713	801
Strain (%)	2.01	2.00	1.99	1.98
	2.01	2.00	2.00	2.01
	2.00	2.00	2.00	2.00
	2.01	2.00	2.00	2.00
Time From Cutting (hrs)	2.01	1 1 1	1	1 1 1
Distance From Bondline (in.)	0.1	0.5	1.0	2.0

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TABLE 8

8

MOTOR TC 30033 STRESS RELAXATION GRADIENT ANB-3066 PROPELLANT, FORWARD EQUATOR AREA, AMBIENT SEGMENT 2L2 7-YEAR (1985) RESULTS

1.30	223	737 461	488	476	644	335	420	285	327	$\frac{337}{316}$		342	385	382
(psi)	27.0	57.5 511	543 475	533	667	370	467	320	363	376	}	382	413	481
Log Time (min	23.0	430 583	623 545	919	575	438	543	375	426	$\frac{433}{411}$!	777	493	252 496
Relaxation Modulus (psi) Log Time (min) -0.34 0.20 0.86	70,	668	705 623	782	658	492	779	439	503	502 481	ļ	516	5/0	635 574
-0.03	611	800	841 751	936	804	621	787	554	663	618	! ! •	635	00/	702
Strain (2)		2.00	$\frac{2.00}{2.00}$	1.99	2.01	2.00	2.00	2.00	2.01	2.00) 	1.98	2.00	$\frac{2.01}{2.00}$
Time From Cutting (hrs)	(III.9)	ı		1				l				ı		
Distance From Bondline (in.)	100	1.0		0.5				1.0				2.0		

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TOTAL TOTAL RESIDENCE TOTAL SECTION OF

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TABLE 9

PROPELLANT SHORE A HARDNESS, 15-SECOND READINGS FORWARD FLAP AREA, SEGMENT 1B6, AREA A 7-YEAR (1985) RESULTS

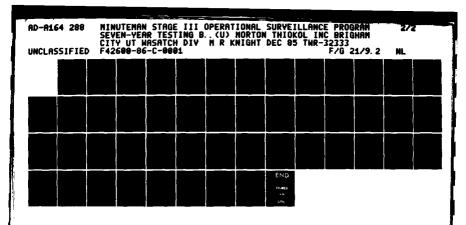
Distance From		Motor	
Bondline (in.)	TC 30005	TC 30019	TC 30033
0.1	44±1.1 ¹	44±1.0	50±1.53
0.2	50±1.0	47±0.0	55±1.1
0.3	51±0.6	48±0.6	57±0.6
0.4	52±0.6	46±0.0	60±1.1
0.5	51±1.0	48±0.0	60±1.0
0.6	53±0.6	48±1.5	62±0.6
0.7	60±0.0	50±2.1	63±1.0
0.8	61±0.6	51±1.1	64±0.6
0.9	60±0.6	51±1.1	63±0.6
1.0	61±0.6	53±1.5	64±1.0
1.1	61±0.6	57±1.5	64±1.0
1.2	60±1.0	58±2.0	64±1.0
1.3	59±1.0	59±0.6	64±0.6
1.4	58±0.6	61±1.7	66±0.6
1.5	55±0.6	63±1.0	65±0.0
1.6	52±0.6	63±0.6	63±0.6
1.7	50±0.0	64±0.6	62±1.0
1.8	49±1.5	63±1.0	61±1.1
1.9	46±0.6	64±0.6	60±0.0
2.0	45±1.0	64±0.6	61±0.6

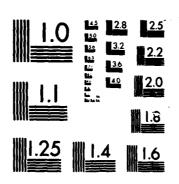
¹Standard Deviation for Triplicate Tests

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MICROCOPY RESOLUTION TEST CHART

TABLE 10

PROPELLANT SHORE A HARDNESS, 15-SECOND READINGS FORWARD FLAP AREA, SEGMENT 1B6, AREA B 7-YEAR (1985) RESULTS

Distance From		Motor	
Bondline (in.)	TC 30005	TC 30019	TC 30033
0.1	65±0.6 ¹	57±0.6	59±1.1
0.2	65±1.1	59±1.0	61±0.6
0.3	65±0.6	59±1.1	62±1.0
0.4	64±1.0	57±1.0	61±0.6
0.5	65±2.1	57±0.6	59±1.0
0.6	64±1.0	55±0.6	58±0.6
0.7	65±0.6	54±0.6	56±0.6
0.8	62±0.6	56±2.1	55±0.0
0.9	60±0.6	55±0.6	56±0.6
1.0	60±0.6	55±0.6	55±0.0
1.1	59±0.6	56±1.0	56±0.6
1.2	58±0.0	56±0.6	55±0.6
1.3	57±0.0	57±1.1	54±0.6
1.4	58±0.6	56±1.0	52±0.0
1.5	58±0.6	58±0.6	53±0.6
1.6	56±0.0	60±1.0	50±0.6
1.7	54±0.6	60±0.6	49±0.0
1.8	54±0.6	59±0.6	47±0.6
1.9	54±0.0	60±0.6	47±1.0
2.0	52±0.0	60±1.0	46±0.6

¹Standard Deviation for Triplicate Tests

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TABLE 11

PROPELLANT SHORE A HARDNESS, 15-SECOND READINGS
FORWARD FLAP AREA, SEGMENT 1B6, AREA C
7-YEAR (1985) RESULTS

Distance From		Motor	
Bondline (in.)	TC 30005	TC 30019	TC 30053
0.1	54±0.6 ¹	60±0.6	57±2.3
0.2	53±0.0	64±0.6	59±0.6
0.3	50±0.0	67±0.6	58±1.0
0.4	45±0.6	67±0.6	58±0.6
0.5	43±0.6	65±0.6	58±0.6
0.6	41±0.6	61±0.6	59±0.6
0.7	42±0.0	60±0.6	61±0.6
0.8	41±0.6	58±0.6	62±0.0
0.9	42±0.6	58±0.6	64±0.6
1.0	43±0.0	56±1.0	67±0.0
1.1	43±0.6	55±0.6	67±0.6
1.2	43±0.6	54±0.6	66±0.6
1.3	40±0.6	55±0.6	65±0.6
1.4	39±0.6	56±0.6	65±0.0
1.5	38±0.6	55±0.6	63±0.6
1.5	40±0.6	56±0.6	60±0.6
1.7	39±0.6	57±0.6	57±0.0
1.8	41±0.6	56±0.6	55±0.6
1.9	42±0.6	57±0.6	54±1.0
2.0	43±0.6	57±0.6	52±0.6

Standard Deviation for Triplicate Tests

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V-45 RUBBER MATERIAL PROPERTIES DATA FORWARD FLAP AREA, SEGMENT 186 7-YEAR (1985) RESULTS

×				NO. THRE 32333	PAGE 87
	Motor No.	TC 30005	TC 30019	€ TWR-32333	اسا
	V-45 Swell Ratio	1.56 1.61 1.32 1.27 1.27 1.39	1.30 1.33 1.36 1.37	1.35 1.37 1.37 1.37	1.34 1.35 1.35
	V-45 Moisture (%) (Azocotropic)	1 1 1	1 1 1	1 1 1	
	V-45 Moisture (%) (Dupont)	1.46 1.22 $\frac{1.12}{1.27}$	1.45 1.31 1.43 1.40	1.09 1.10 1.25	1.15
	V-45 DOP (2)	1.21 1.17 1.15 1.18	$ \begin{array}{c} 1.14 \\ 1.21 \\ 1.17 \\ 1.17 \end{array} $	1.19 1.27 1.30	1.25
:	V-4> 15-Second Shore A Hardness	61 62 62	65 88 86 86	65 67	99

TABLE 13

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MOTOR TC 30005 MATERIAL PROPERTIES DATA 7-YEAR (1985) RESULTS

	Mir	Mini DPT			Liner	Liner	Liner
	Maximum	Failu	Failure Mode (%)	e (%)	Swel1	Ge1	Moisture
Sample Area	Stress (ps1)	APL	리	GL	Ratio	Fraction	(%)
	77	20	80		1.82	0.443	Not Required
Segment 1B6	77	40	09		1.88	0.457	i
	23	0	100		1.88	0,440	
	29	0	100		1.94	0.337	
	31	0	100		1.94	0.466	
	33	30	70		1.94	0.412	
	35				2.13	0.375	
					2.06	0.374	
					2.13	0.385	
)		
Barrel, Between		Not Required This	red Th	is Year			

Barrel, Between Not Required This Year
Ground Straps
Barrel, Under Not Required This Year
Ground Straps

Not Required This Year

Aft Flap

TABLE 14

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MOTOR TC 30019 MATERIAL PROPERTIES DATA 7-YEAR (1985) RESULTS

Liner	Moisture	(%)	Not Required	•							
Liner	Ge1	Fraction	0.413	0.405	0.383	0.414	0.347	0.313	0.260		
Liner	Swell	Ratio	2.26	2.19	2.26	2.11	2.06	2.08	2.25		
Mini DPT	Maximum Failure Mode (%)	Stress (psi) APL CL CLI	34 0 100 -	26 0 100 -	38 0 100 -	36 0 100 -	0	$\frac{41}{}$ 0 100 -	34	Not Required This Year	Not Required This Year
		Sample Area	Forward Flap	Segment 1B6						Barrel, Between Ground Straps	Barrel, Under Ground Straps

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Aft Flap

Not Required This Year

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TABLE 15

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MOTOR TC 30033 MATERIAL PROPERTIES DATA 7-YEAR (1985) RESULTS

Liner	Moisture	(%)	Not Required						
Liner	Ge1	Fraction	0.404	0.432	0.417	0.395	0.548	0.465	
Liner	Swel1	Ratio	2.47	2.47	2.11	2.16	2.00	2.05	i i i
Mini DPT	Failure Mode (%)	APL CL CLI	0 100 -	0 100 -		10 90 -	0 100 -	0 100 -	
M	Maximum	Stress (psi)	35	35	45	26	22	39	\$
		Sample Area	Forward Flap	Segment 1B6	ı				

Barrel, Between Ground Straps

Not Required This Year

Barrel, Under Ground Straps Not Required This Year

Not Required This Year

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TABLE 16

MOTOR TC 30005 LINER PENETROMETER DATA FORWARD EQUATOR PROFILE, SEGMENT 2L2, 10-SEC READINGS 76°F, 7-YEAR (1985) RESULTS

	1	Penetration (10	
Distance	Standard		Fine Needle
Aft of	100g	No	No
Equator (in.)	Weight	Weight	Weight
-1	68	37	51
1	32	17	22
3	48	29	32
5	62	34	35
7	53	31	31
9	60	33	37
11	76	39	47

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TABLE 17

MOTOR TC 30019 LINER PENETROMETER DATA FORWARD EQUATOR PROFILE, SEGMENT 2L2, 10-SEC READINGS 76°F, 7-YEAR (1985) RESULTS

	1	Penetration (10) mm)
Distance	Standard	Needle	Fine Needle
Aft of	100g	No	No
Equator (in.)	Weight	Weight	Weight
-1	42	32	35
1	33	18	21
3	48	22	31
5	47	21	29
7	58	34	41
9	59	34	36
11	68	39	46

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TABLE 18

MOTOR TC 30033 LINER PENETROMETER DATA FORWARD EQUATOR PROFILE, SEGMENT 2L2, 10-SEC READINGS 76°F, 7-YEAR (1985) RESULTS

	I	Penetration (10) ⁻¹ mm)
Distance	Standard	Needle	Fine Needle
Aft of	100g	No	No
Equator (in.)	Weight	Weight	Weight
, -1	48	30	49
1	44	23	24
3	53	30	35
5	59	33	34
7	58	32	38
9	57	27	33
11	68	38	44

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TABLE 19

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MOTOR TC 30005 STRESS RELAXATION GRADIENT ANB-3066 PROPELLANT, FORWARD FLAP AREA, AMBIENT INDIVIDUAL RESULTS, SEGMENT 1B6 7-YEAR (1985) TESTS

	1.30	352 396	349	447	494 451 464	500 541	$\frac{531}{524}$
s (ps1)	0.80	401	398 416	510	513 528	562 609	579 583
Relaxation Modulus (ps1) Log Time (min)	0.20	477 526	470	596	608 620	659 712	$\frac{673}{681}$
Relaxati	-0.34	567 620	561 583	700	723 731	769 806	780 785
	-0.93	590	713	862	944 901 902	940	956 957
Strain	(%)	2.00	$\frac{2.01}{2.00}$	2.00	2.00	2.00	$\frac{1.99}{2.00}$
Time From Cutting	(hr)	2.2	3.0	2.8	3.2	3.01 3.8	3.8
Distance From Bondline	(in.)	0.1		0.3		0.5	

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TABLE 20

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ANB-3066 PROPELLANT, FORWARD FLAP AREA, AMBIENT INDIVIDUAL RESULTS, SEGMENT 1B6
7-YEAR (1985) TESTS

Distance From Bondline	Time From Cutting	Strain	Ì	Relaxation Modulus (Log Time (min)	Relaxation Modulus (psi) Log Time (min)	(psi)	
(in.)	(fr)	$\overline{(\frac{7}{8})}$	-0.93	-0.34	0.20	0.80	1.30
0.1	3.1	2.00	1010	676	685	578	506
	3.1	2.00	905	717	602	502	451
	1.5	•	866	684	578	491	435
		2.00	926	783	622	524	797
0.3	3.7	1.99	1120	915	782	661	591
	3.7	1.98	984	797	619	610	909
	2.1	2.01	1030	841	721	618	549
		2.00	1045	851	727	630	249
0.5	ı	•	1150	943	814	269	628
	3.9	2.01	991	814	703	909	240
	2.3	2.02	1060	868	748	645	<u>561</u>
		7.01	7007	۵/۶	(2)	649	۲/ ۲

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MOTOR TC 30033 STRESS RELAXATION GRADIENT ANB-3066 PROPELLANT, FORWARD FALP AREA, AMBIENT INDIVIDUAL RESULTS, SEGMENT 1B6 7-YEAR (1985) TESTS

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	1.30	312	308	416	421	<u>549</u> 462	489	490	491 490
(psi)	1		337						
Relaxation Modulus (psi) Log Time (min)	0.20	452	1 427 3 432	565	561	$\frac{739}{622}$	651	565	647 621
Relaxatio	-0.34	544	521 523	871	299	882 807	762	743	738
	-0.93	708	683 681	778	821	1110 925	935	904	935 925
Strain	(%)	2.00	2.01	1.90	1.99	$\frac{2.00}{1.99}$	1.98	2.02	$\frac{2.00}{2.00}$
Time From Cutting	(hr)	2.0	2.2	2.2	2.7	2.9	3.0	3.0	ı
Distance From Bondline	(in.)	0.1		0.3			0.5		

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TABLE 22

PROPELLANT SHORE A HARDNESS, 15-SECOND READINGS
FORWARD EQUATOR AREA, SEGMENT 2L2
7-YEAR (1985) RESULTS

Distance From		Motor	
Bondline (in.)	TC 30005	TC 30019	TC 30033
0.1	66±0.6 ¹	61±1.5	62±0.0
0.2	63±1.0	63±1.1	61±1.0
0.3	63±1.0	57±0.6	60±0.6
0.4	64±0.6	56±1.5	59±1.0
0.5	61±1.1	52±0.6	56±1.0
0.6	60±0.6	50±0.6	55±0.6
0.7	57±0.6	50±0.6	54±0.0
0.8	57±0.6	48±0.6	53±0.0
0.9	57±0.0	48±1.0	52±1.0
1.0	57±0.6	48±0.6	53±1.1
1.1	58±0.6	50±0.6	53±1.1
1.2	57±1.0	50±0.6	54±1.1
1.3	56±1.1	52±0.6	53±0.0
1.4	57±1.5	53±1.0	54±0.0
1.5	57±1.0	53±0.6	54±0.6
1.6	57±1.0	53±0.6	54±0.6
1.7	58±0.6	55±0.0	54±1.0
1.8	58±0.6	55±0.6	54±0.6
1.9	59±1.5	54±0.0	55±0.0
2.0	59±1.0	55±0.6	55±0.0

 $^{^{\}mathrm{l}}$ Standard Deviation for Triplicate Tests

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1.

MATRIX FOR SURVEILLANCE TESTING OF STAGE III MINUTEMAN MOTOR TC 30024

Test Schedule	Monthly	Honthly	Monthly	Every 6 months	Every 6 months	Inspection monthly
Tests	Forward gap measurement	Mipple movement ²	Aft bore diameter measurement	Radiographic inspection 4	Shore A propellant readings ⁵	Liner runs (document as required)
Test Condition	Temperature 70 + 5°P.	Bunidity 50 + 5% RH.	Motor stored in vertical	mode, aft end down		

Every 90 degrees

Observed, measured, and documented as required

Ressured two places 90 degrees apart

Saft end of motor nozzle well every 60 degrees, 5 places (omit excise sample location at 60 degrees) Angent line bonds, forward and aft separations, x-ray in two modes aft down, forward down

6 Document (photograph) as required. Weigh significant accumulations as required.

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TABLE 24

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MATERIAL PROPERTIES OF SAT-CONDITIONED MOTOR TC 30050 SECHENTS: STORE WITH MOTOR TC 30024, TEST AT 2-YEAR INTERVALS

# # # # # # # # # # # # # # # # # # #	Motor	Segment Identification and Test Date	Material	Material Property	Test Conditions	Specimen	Number/ Interval
B6C3 in 1981, B6C4 in 1983, B6C4 in 1981, B6C4 in 1983, B6C4 in 1983, B6C4 in 1981, B6C4 in 1983, B6C4 in 1981, B6C4 in 1983, B6C4 in 1983, B6C4 in 1983, B6C5 in 1983, B7C6 in 1983, B7C7 in 1983, B7	Forward Equator Between	A2E (1/3) in 1981, A2E (1/3) in 1983, A2E (1/3) in 1985	ANB-3066/ SD-851-2/ V-45	Bond Tensile Profile	0.5 in/min	Mini DPT	71
B6C3 in 1981, ANB-3066/ Bond Tensile 0.5 in/min 2064 in 1983, V-45 B6C4 in 1983, V-45 B6C4 in 1983, V-45 BCC4 in 1983, SD-851-2/ Profile 0.5 in/min 2064 in 1981, ANB-3066/ Bond Tensile 0.5 in/min 2064 in 1981, ANB-3066/ Bond Tensile 0.5 in/min 2064 in 1981, ANB-3066 Uniaxial 1.0 in/min 2068 in 1983, SD-851-2 Swell Ratio 2 Gel Fraction 2 Gel Fraction 2 Gel Fraction 2 Gel Fraction 2 Shore A4 15-Second 2 Sho	Grounding Straps		SD-851-2	Swell Ratio	;	•	ដ
B6C3 in 1981, SD-851-2/ Profile B6A3 in 1983, SD-851-2/ Profile B6C4 in 1985, V-45 BCC4 in 1985, V-45 BCC4 in 1985, SD-851-2 Gel Fraction BC3F (1/2) in 1981, ANB-3066/ Bond Tensile 0.5 in/min BC3F (1/2) in 1985 V-45 Ce F4B1 in 1981, ANB-3066 Uniaxial F4F1 in 1981, ANB-3066 Uniaxial F4F1 in 1983, SD-851-2 Swell Ratio Gel Fraction ² F4B2 in 1983, SD-851-2 Swell Ratio Gel Fraction ² F4B2 in 1983, SD-851-2 Swell Ratio Gel Fraction ² F4B2 in 1983, SD-851-2 Swell Ratio Gel Fraction ² F4B2 in 1983, SD-851-2 Swell Ratio F4B2 in 1985, SD-851-2 Swell Ratio				Gel Fraction Profile ²	:	:	\$2
DE3F (1/2) in 1981, ANB-3066/ Bond Tensile 0.5 in/min DE3F (1/2) in 1983 SD-851-2/ DE3F (1/2) in 1985 V-45 Ce F4B1 in 1981, ANB-3066 Untaxial 1.0 in/min F4B1 in 1983, Shore A ⁴ 15-Second	Aft Flap	B6C3 in 1981, B6A3 in 1983, B6C4 in 1985	ANB-3066/ SD-851-2/ V-45	Bond Tensile Profile	0.5 in/min	Mtnf DPT	13
DE3F (1/2) in 1981, ANB-3066/ Bond Tensile 0.5 in/min 2E4B1 in 1983 SD-851-2/ Swell Ratio Gel Fraction ² Ce F4B1 in 1981, ANB-3066 Uniaxial 1.0 in/min F4B1 in 1983, Shore A ⁴ 15-Second			SD-851-2	Gel Fraction Profile ³	:	:	1 2
Ce F4B1 in 1981, ANB-3066 Uniaxial 1.0 in/min F4B2 in 1983, Shore A ⁴ 15-Second	Barrel Between and Under		ANB-3066/ SD-851-2/ V-45	Bond Tensile	0,5 in/min	Man DPT	•
in 1981, AMB-3066 Uniaxial 1.0 in/min in 1983, Tensile ⁴ is 15-Second in 1985	Grounding Straps		SD-851-2	Swell Ratio Gel Fraction ²			12
in 1985 15-Second	Bore Surfac		ANB-3066	Uniexial Tensile ⁴	1.0 in/min	Mini Tensile	21
		F4B2 in 1985		Shore A4	15-Second	•	21

All tests at 77°F, ambient pressure.

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Obtain from swell ratio specimens where possible and also from tested mini DFT specimens.

30btain from tested mini DPT specimens where possible.

⁴Test 3 each at 0.1, 0.2, 0.3, 0.4, 0.5, 1, and 2 in. from bore surface.

TABLE 25

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MINI DPT BOND STRENGTH PROFILE OF MOTOR TC 30050 SAT SEGMENTS AT FIRING OF MOTOR TC 30106 AND 5.5 YEARS LATER

Í	CLI	Later	ı	ſ	1	ſ	1	ı	ı	ı	•	ı	ı	ı	ı	,	1	1	į	1
	Į	A.F.	ı	,	1	ı	ı	ı	j	ı	30	20	15	15	1	1	10	20	10	10
e Mode	١	Later	ì	100	100	100	100	100	100	100	100	20	20	20	100	100	100	30	20	10
Failure Mode	IJ	A.F.	100	100	100	100	100	100	100	40	ı	ı	,	,	100	06	45	J	1	ı
	APL	Later	ı	ı	ı	ı	ı	ı	ı	ı	ı	80	80	20	ı	ı	1	70	80	06
		A.F.	1	ı	ı	١	í	1	ı	09	70	80	85	85	ı	10	45	80	90	06
Maximum Stress (psi)	5.5 Years	Later	1	16	17	11	14	18	14	18	34	89	59	50	14	16	22 17	83	85	85 84
Maximum S	At	Firing	11	17	14	18	10	7	12	37	61	91	98	89	37	48	4 <u>7</u> 4 <u>7</u>	66	91	76 89
Distance Aft	of Forward	Equator (in.)	-7	9-	-5	7-	-3	-5	7	0	7	2	3	4	25 A.F.	14 Later		25 A.F.,	14 Later	
		Location	Forward	Equator,	Between	Grounding	Straps								Barrel,	Between	Grounding Straps	Barrel,	Under	Grounding Straps
																0	oc o. TWI	<u>-3</u> 2	23:	33

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TABLE 25 (CONTINUED)

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MINI DPT BOND STRENGTH PROFILE OF MOTOR TC 30050 SAT SEGMENTS AT FIRING OF MOTOR TC 30106 AND 5.5 YEARS LATER

	Distance Aft	MaximixeM	tress (psi)			Failu	Failure Mode	!	İ
	of Forward	At	5.5 Years	1	.PL	To			CLI
Location	Equator (in.)	Firing	Firing Later	A.F.	T. Later	A.F.	Later	A.F. Lat	Later
Aft Flap	-11	1	15	ı	í	ı	100	•	•
	-10	ı	15	•	í	1	100	ı	ı
	6-1	1	19	ı	1	ι	100	1	1
	. φ	ī	25	1	ı	1	100	1	t
	7-	•	10	1	ı	ı	100	ı	•
	91	1	7	1	ı	1	100	ı	t
	- 5	1	7	1	1	1	100	ı	1
	· m	1	13	ı	ł	1	100	1	ı
	*0	ı	ı	ı	•	1	1	ı	i
	2*	ı	ı	1	ı	1	ı	1	1
	% *	ı	ı	t	1	ı	ı	ı	1
	**	•	ı	•	,	1	•	1	1

*Liner too degraded to test.

NOTE: All aft flap sample liner had degraded.

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TABLE 26

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LINER GEL FRACTION AND SWELL RATIO PROFILES OF MOTOR TC 30050 SAT SEGMENTS AT FIRING OF MOTOR TC 30106 AND 5.5 YEARS LATER

Liner Swell Ratio At 5.5 Years	Later	*	*	*	*	*	*	*	2.08	1.88	2.08	2.18	*			*		
Liner S At	Firing	*	*	*	*	*	*	1.97	1.85	1.73	1.82	1.91	*			1.90	1.91	1.94
Liner Gel Fraction 5.5 Years Later	From Swell Samples	0.184	0.185	0.304	0.275	0.291	0.079	0.299	ı	ı	1	1	0.340	0.153	$\frac{0.253}{0.249}$	0.557	0.469	0.446
Liner Ge	From Mini DPTs	0.240	0.250	0.234	0.229	0.239	0.052	0.329	0.466	0.562	0.517	0.488	0.622	0.464	0.435	0.597	0.615	0.608
At	Firing	0.139	0.140	0.051	0.047	0.062	0.127	0.419	0.522	0.617	0.550	0.518	0.222	0.257	$\frac{0.251}{0.243}$	0.552	0.563	0.535
Distance Aft of Forward	Equator (in.)	9-	-5	7-	۳-	-2	7	0	1	2	m	7	25 A.F.,	14 Later		25 A.F.	14 Later	
	Location	Forward	Equator,	Between	Grounding	Straps							Barrel,	Between	Grounding Straps	Barrel.	Under	Grounding
•															DOC NO.	TWR	-3	233

TABLE 26 (CONTINUED)

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LINER GEL FRACTION AND SWELL RATIO PROFILES OF MOTOR TC 30050 SAT SEGMENTS AT FIRING OF MOTOR TC 30106 AND 5.5 YEARS LATER

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Liner Swell Ratio At 5.5 Years Tring Later	*											
Liner S At Firing	1 1	1	ı	1	1	ı	•	ı	1	1	1	ı
Liner Gel Fraction 5.5 Years Later From Mini DPTs From Swell Samples	*											
Liner Ge 5.5 Ye From Mini DPTs	0.056	0.044	0.037	0.050	0.035	0.036	0.087	0.257	0.084	0.069	0.073	0.080
At Firing	1 1	ı	ι	ı	ı	ı	1	1	ſ	ı	ı	ı
Distance Aft of Forward Equator (in.)	-11 -10	6-	891	-7	9-	-5	-3	-	2	m	7	2
Location	Aft Flap											

*Liner too degraded to test.

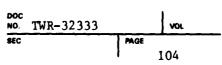
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TABLE 27

BORE PROPELLANT MINI TENSILE AND SHORE A GRADIENTS OF MOTOR TC 30050 SAT SEGMENTS AT FIRING OF MOTOR TC 30106 AND 5.5 YEARS LATER

Distance From Bore	E1.0	E ^{1.0} (psi)	α) " β	si)	£3.0	(%)	1.0	(%)	15-Sec 8	hore A
Surface (in.)	A.F.	Later	A.F. Later	Later	A.F.	A.F. Later	A.F. Later	Later	A.F. Later	Later
0.1	1800 ± 62^{1}	1800±62 ¹ 1811±528	153±4.0 162±54	162±54	17±0.6	17±0.6 14±0.8	20±1.1	20±1.1 20±2.9	71±2.6	71±2.6 67±0.6
0.2	1820±85	1525±217	151±2.3 134±18	134±18	15±0.0	15±0.0 14±0.2	19±1.5 20±2.0	20±2.0	74±0.6	74±0.6 68±0.6
0.3	1760±87	1443±423	151±5.1 132±33	132±33	15±0.0	15±0.0 15±0.2	18±0.0 20±0.1	20±0.1	73±1.0	73±1.0 67±0.0
0.4	1700±20	1507±77	154±3.5 150±2	150±2	15±0.0	15±0.0 15±0.4	18±0.6 18±0.9	18±0.9	72±0.0	72±0.0 68±1.5
0.5	1650±111	1436±73	155±4.0 152±3	152±3	15±0.6	15±0.6 15±0.3	19±0.0 19±0.6	19±0.6	72±0.6	72±0.6 66±2.0
1.0	1340±56	878±86	141±3.2 132±3	132±3	20+0.0	20±0.0 22±1.3	25±0.6 27±1.5	27±1.5	68±1.0	68±1.0 63±0.6
2.0	1220±15	565±20	134±2.0 110±3	110±3	24±0.6	24±0.6 29±0.4	28±3.2	28±3.2 40±2.1	63±0.6 60±0.6	9.0±09

¹Standard Deviations for Triplicate Tests



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DISSECTED MOTOR IC 30072 SECMENT TEST DATES

Aft Flap	6B, 6D, 6F	None	V9	None	ວ9	None .	3 9
Aft Equator*	5B, 5E, 5H	5D	51	SG	50	5A	58
Barrel Between, Under and Bore Surface	3B, 3E, 3H	37	3A	Н7	30	48	36
Forward	2B, 2F, 2J	None	2 L	None	2Ω	None	24
Forward Flap*	101	1C2	141	1E2	101	181	121
Forward	18, 1D, 1F	None	14	None	10	None	1E
Years From Dissection	Baseline**	ч	2	e	7	'n	\$
Test	1983	* 7861	1985*	1986*	1987*	1988*	1989*

*Denotes tests not included in Addendum #1

**Except for testing of Forward Flap Segment, baseline testing will be at three locations, namely 60, 180 and 300 degrees.

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TABLE 29

MATERIAL PROPERTIES TESTING OF DISSECTED OPERATIONAL MOTOR SECHENTS

V-45 Swell Retto	t	1 Area	Areas A	1	ł	1	Areas A and C	Area 7
V-45 Plasticizer	1 Area	1 Area	Afeas A and C	ı	i	ł	Areas A and C	Area P
V-45 Moisture			Areas A and C	1 Area ³	1 Area	1	Areas A and C	Area F
272	1 Area	1 AFEA	3 Areas	1	1	1	3 Areas	Area 7
Propellanc Shore A Gradient	;	1	t	1	ı	1 Area	1	ı
Propellant Mini Tensile Gradient		1	1	1	1	1 Area	1	1
Propellant Er Gradient	1 Area	1 Area	3 Areas	1 Area	1 Area	1	3 Acres	3 Areas
Liner C=0/C=C Ratio	1 Area	1 Area	Profile1	1 Area ⁵	1 Area ⁵	1	Profile ³	3 Areas
Liner Swell Ratio	ł	1 Area	Profile1	1 Area ⁵	1 Area ⁵	ı	Profile3	Profile.
Liner Cel Fraction	1 Area	1 Area	Profile 1	1 Area 1 Area	1 Area ⁵	ł	Profile ³	Profile
i		1 AFEA	Profile	1 Area	1 Areas	1	Profile ³	Profile.
1	Alan Lines	Forused Flap	Forward Equator Between Strape	Barrel Between Straps	Barrel Under Scraps	Bore Surface	Aft Equator Between Strape	Aft Plap

At 1-inch intervals from 7 inches forward to 4 inches aft. TWR-32333

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Plus hinge bulb gradient.

At 1-inch intervals from 4 inches forward to 7 inches aft.

PAGE

At 1-inch intervals from tip to il inches forward.

baseline tests at 60-degree location will be a profile at 1-inch intervals from center of grounding strip to center of area between grounding atribe.

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TABLE 29

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MATERIAL PROPERTIES TESTING OF DISSECTED OPERATIONAL MOTOR SECRENTS

							Propellant		1	:	
		Liner Cel Fraction	Liner Swell Racto	C=0/C=C	Propellant Er Gradient	Tenaile Gradient	Shore A Gradient	V-45 Er	V-45 Molsture	닖	Swell Ratio
Motor Location	שומי מני								. 4	Area	;
Forward Nipple	ł	1 Area	1	1 Area	1 Area	i		1 160		! :	
Forward Flap	1 ATOR	1 Area	1 Area	I Area	1 Area	ı	í	1 Area	1 Arcs	1 AFRE	l Area
Forward Equator Between Strape	Profile ¹	Profile.	Profile ¹	Profile1		t	ŧ	3 AFOAS	Areas A	Areas A	Areas A
Barrel Between Straps	1 Area	1 Area	1 Area ⁵	1 Area ⁵	1 Area	ı	ŧ	1	1 Areas	i	1
Barrel Under Straps	1 Area	1 Area ⁵	1 Area ⁵	1 Area ⁵	1 Area	ı	ı	ţ	1 Area		l
Bore Surface	1	ı	i	ŧ	1	1 Area	1 Area	;		I	1
Afc Equator Between Straps	Profile ³	Profile ³	Profile ³	Profile ³	3 Areas	1	1	3 Areas 2	Areas A and C	Areas A	Areas A and C
Aft Flap	Profile	Profile ⁴	Profile*	3 Areas	3 Areas	1	ł	Area 7	Area F	AFEA P	Ared P

At 1-inch intervals from 7 inches forward to 6 inches aft.

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Plus hinge bulb gradient.

3c 1-inch intervals from 4 inches forward to 7 inches aft.

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At 1-inch intervals from tip to 11 inches forward.

Sassifue tests at 60-degree location will be a profile at 1-inch intervals from center of grounding strip to center of area between grounding stripe.

TABLE 30

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MATERIAL PROPERTY TESTS FOR DISSECTED MOTOR SEGMENTS (1)

cimens	BOIL	m	က	ო	-	01	21	21	က	ო	က	ო	က	0,4, 0.5, 1 and stee, in middle
Number Specimens	Froirie	96	13	77	77	1	ţ	;	1	ł	13	ł		0.3. irface iterface ipilit
	Specimen Type	Mini DPT	ţ	i	1	Mini Er (0.1x0.5x2 in.)	Mini Tensile	ţ	Mini E _r (th.x0.5x4 in.)	Mini E _r (0.lx0.5x4 in.)	ł	ł	1	Test at 0.1, 0.2, 0.3, 0.4, 2 in. from bore surface Test near liner interface, of bulb and near split By Dupont Moisture Analyzer
	Conditions	0.002, 0.5, 20 in/min	1	;	;	2% strain	1 in./min.	15 sec	2% strain	8	;	3	•	(5) from (7)
	lest lype	Bond Tensile	Gel Fraction	Swell Ratio	C-0/C-C Ratio ⁽²⁾	Stress Relaxation Gradient (3,4)	Uniaxial Tensil63,5)	Shore A Gradient (5)	Stress Relaxation (3)	Stress Relaxation Gradient (6)	Moisture Content (7)	Plasticizer Content	Swell Ratio	All tests at 77°F, 0 paig By ATR/FIR using tested mini DFT specimens Test samples in hoop orientation Test at 0.1, 0.3, 0.5, 1, and 2 in. from liner interface
•	Material	ANB-3066/ SD-851-2/ V-45	SD-851-2			ANB-3066			V-45					(1) All tes (2) By ATR/F (3) Test sa (4) Test at liner i
REVIS	BION _								Di No	oc TWR-	3233	3		vor

MATERIAL PROPERTIES (BASELINE TESTS ONLY, OF SEGMENTS FROM DISSECTED MOTOR

Ú

Number of	m	375 3	75 2	en en	E A	m
Specimen Type	4 x 0.5 x 0.5 Tab End	2 x 0.375 x 0.375	4 x 0.75 x 0.75 Tab End	JANNAF Class B	JANNAF Class B	Disk Tab End
Test Conditions	-30 ^o F, 2% strain, 600 psi	0° to 145°F, 0 ps1	77°F, O psi	180°F, 0.002 in/min, 0 psi	30°F, 200 in/min, 600 psi	30°F, 20 in/min, 400 psi
Test Type	Relaxation Modulus	TCLE	Poisson's Ratio	Strain at Maximum Stress	Strain at Rupture	Bond Shear Strength
Material	ANB-3066 Propellant (Bore Area)					V-45/EC2216/V-45 (Tangent Line Area)

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MOTOR TC 30072 BOND STRENGTH AND LINER PROPERTIES IN FORWARD NIPPLE AND FORWARD FALP AREAS 2-YEAR (1985) RESULTS

REVISION _		MOIOK IC 30072 BOND SIKENCIH AND LINEK PROPEKTIES IN FORWARD NIPPLE AND FORWARD FALP AREAS 2-YEAR (1985) RESULTS	7072 BOND VARD NIPP 2-YEA	BOND SIKENCIH AND LIR NIPPLE AND FORWARD F4 2-YEAR (1985) RESULTS	H AND L ORWARD RESULT	K 1C 30072 BOND SIRENGIH AND LINER PROPE. IN FORWARD NIPPLE AND FORWARD FALP AREAS 2-YEAR (1985) RESULTS	RTIES		
	Mini	Mini DPT Bond Strength (psi)	Strength	(psi)		Liner	Liner	Liner C=0/C≈C Ratios	Ratios
Motor Location	Rate (in./min)	σm (psi)	Failu APL	Failure Mode (%) PL CL CL	(%) CLI	Gel Fraction	Swell Ratio	C=C Stretching	C=C Vinyl
Forward Nipple:									
Segment 1A		Not Required	juired			0.524 0.535 0.495 0.518	Not Required	0.559	0.116
Forward Flap:									
Segment 1A1	0.002 0.5 20	20 45 74	100	100	1 1 1	0.479 0.499 0.436 0.470	$\begin{array}{c} 1.89 \\ 1.94 \\ 1.97 \\ 1.93 \end{array}$	0.568	0.117

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TABLE 33

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MOTOR IC 30072 BOND STRENGTH AND LINER PROPERTIES IN FORWARD EQUATOR AREA, SEGMENT 2L, BETWEEN GROUNDING STRAPS 2-YEAR (1985) RESULTS

C Ratios C=C Vinyl	0.101	0.101	0.111	0.130	0.118	0.120	0.144
Liner C=0/C=C Ratios C=C C=C Stretching Vinyl	0.512	0.501	0.519	0.560	0.560	0.587	0.701
Liner Swell Ratio	2.25±0.0	2.31±0.03	2.29±0.01	2.10±0.01	2.24±0.01	2.18±0.05	2.27±0.12
Liner Gel Fraction	0.445 ± 0.06^{1}	0.437±0.04	0.425±0.03	0.561±0.07	0.483±0.04	0.516±0.02	0.476±0.02
(%) CLI	1 1 1	1 1 1	1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
Strength Failure Mode APL CL	100 100 20	100 100 100	100 100 10	95 80 50	90 40	30 10	06 1 1
Failu APL	- 1 80	1 1 1	1 1 06	5 20 50	10 60 100	40 70 80	10 100 100
OPT Bon Om (psi)	10 30 73	15 35 68	13 33 75	19 34 77	23 41 75	21 49 82	22 40 73
Mini DPT Bond Strength Rate om Failure Mo (in./min) (psi) APL CL	0.002 0.5 20						
Distance Forward of Forward Equator (in.)	7	9	ď	4	က	2	1
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¹Standard Deviation for Triplicate Tests

TABLE 33 (CONTINUED)

MOTOR TC 30072 BOND STRENGTH AND LINER PROPERTIES
IN FORWARD EQUATOR AREA, SEGMENT 2L, BETWEEN GROUNDING STRAPS
2-YEAR (1985) RESULTS

C Ratios C=C Vinyl	0.162	0.188	0.151	0.155	0.127
Liner C=0/C=C Ratios C=C C=C Stretching Vinyl	0.734	0.714	0.727	0.729	0.671
Liner Swell Ratio	2.01±0.02	1.88±0.04	1.78±0.02	1.89±0.01	2.00±0.03
Liner Gel Fraction	0.569±0.031	0.644±0.01	0.710±0.03	0.645±0.03	0.564±0.07
(%) CLI	1 1 1	i i i	1 1 1	1 1 1	1 1 1
Strength Failure Mode (%) APL CL	1 1 1	06 1	20 40 25	06 1 1	100
Failu	100 100 100	10 100 100	80 60 75	10 100 100	100 100
Mini DPT Bond Strength Om Failure M (psi) APL CL	34 59 103	42 75 124	55 79 129	47 78 94	38 42 112
Mini Rate (in./min)	0.002 0.5 20	0.002 0.5 20	0.002 0.5 20	0.002 0.5 20	0.002 0.5 20
Distance Forward of Forward Equator (in.)	0	7	-5	-3	4-
				DOC	מנות מואת

¹Standard Deviation for Triplicate Tests

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TABLE 34

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MOTOR TC 30072 BOND STRENGTH AND LINER PROPERTIES IN BARREL AREA, SEGMENT 2L, BETWEEN AND UNDER GROUNDING STRAPS 2-YEAR (1985) RESULTS

	Min	DPT Bor	nd Str	ength	-		Liner		Liner C=0/C=0	Ratios
	Rate	ď	Fail	ire l	fode	(%)	Gel		D=0)=O
Motor Location	(in./min)	(psi)	APL	티	CLI	8	(min) (psi) APL CL CLI CP Fraction	Ratio	Stretching Vinyl	Viny1
Between Grounding	0.002	20	50	50	í	1	0.586 ± 0.01^{1}	1.86 ± 0.02	0.635	0.147
Straps, Segment 3A	0.5	99	20	20	ı	1				
	20	116	20	20	t	1				
Under Grounding	0.002	59	50	50	ŧ	ı	0.614±0.00	1.72 ± 0.01	0.717	0.138
Straps, Segment 3A	0.5	79	20	20	ı	ı				
	20	148	20	20	1	ı				

1Standard Deviation for Triplicate Tests.

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TABLE 35

MOTOR TC 30072 BOND STRENGTH AND LINER PROPERTIES IN AFT EQUATOR AREA, SEGMENT 51, BETWEEN GROUNDING STRAPS 2-YEAR (1985) RESULTS

											_	OC O. EC	TWR-	-3	2333	3	F≈	AGE
Distance Aft of Aft	Equator (in.)	7-		-3			-2			7			0			2		
Min	(in./min)	0.002	20	0.002	0.5	20	0.002	0.5	20	0.002	0.5	20	0.002	0.5	20	0.002	0.5	20
ini DPT Bond Strength σ_ Failure M	(psi)	28 54	69	77	29	99	52	88	29	58	86	70	39	99	98	22	51	91
nd Stren Failur	APL	09	95	09	95	95	80	90	95	40	20	90	50	9	06	75	75	100
Strength Failure Mode (%)	립	40	2	70	ς	Ŋ	20	10	Ŋ	09	30	10	20	10	10	25	25	1
(%)	CLI	1 1	ı	ı	ı	ı	1	1	ı	ı	ı	1	ı	1	ı	ı	ſ	1
Liner Gel	Fraction	0.453 ± 0.02^{1}		0.514±0.02			0.579±0.01			0.601±0.01			0.543 ± 0.02			0.494 ± 0.01		
Liner Swell	Ratio	2.01±0.02		2.05 ± 0.03			1.80±0.03			1.81±0.03			2.00±0.0			2.06 ± 0.03		
Liner C=0/C=C Ratios C=C C=C	Stretching	0.579		0.420			0.610			0.469			0.650			0.549		
C=C	Viny1	0.107		0.076			0.130			0.087			0.120			0.105		

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TABLE 36

MOTOR TC 30072 BOND STRENGTH AND LINER PROPERTIES IN AFT EQUATOR AREA, SEGMENT 51, BETWEEN GROUNDING STRAPS 2-YEAR (1985) RESULTS

C Ratios C=C Vinyl	0.108	0.073	0.107	0.122
Liner C=0/C=C Ratios C=C C=C Stretching Vinyl	0.585	0.395	0.564	0.634
Liner Swell Ratio	2.07±0.03	2.09±0.03	2.17±0.0	2.12±0.03
Liner Gel Fraction	0.417 ± 0.02^{1}	0.444±0.04	0.506±0.02	0.424±0.07
(%) a	f f f	1 1 1	1 1 1	1 1 1
Strength Failure Mode (% APL CL CL	75 60 10	90 25 5	30	25 10
Failu Failu	25 40 90	10 75 95	70 95 95	75 90 100
Mini DPT Bond Strength Gm Failure Mc (psi) APL CL	19 40 87	16 50 77	25 53 89	18 58 79
Mare (in./min)	0.002 0.5 20	0.002 0.5 20	0.002 0.5 20	0.002 0.5 20
Distance Aft of Aft Equator (in.)	E	4	\$	9

Standard Deviation for Triplicate Tests

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TABLE 37

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MOTOR IC 30072 BOND STRENGTH AND LINER PROPERTIES IN AFT FLAP AREA, SEGMENT 64, 2-YEAR (1985) RESULTS

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C Ratios C=C Vinyl	0.108	uired	0.120	uired	uired	luired	uired
Liner C=O/C=C Ratios C=C C=C Stretching Vinyl	0.549	Not Required	0.501	Not Required	Not Required	Not Required	Not Required
Liner Swell Ratio	2.16±0.03	2.20±0.14	2.10±0.0	2.10±0.0	2.19±0.05	2.14±0.03	2.08±0.03
Liner Gel Fraction	0.447 ± 0.02^{1}	0.442±0.00	0.538±0.07	0.533±0.04	0.511±0.04	0.502±0.03	0.542±0.03
(%) CLI	1 1 1	1 1 1	1 1 1	1 1 1	20	09	09
Strength Failure Mode APL CL	25 75 50	75 50 5	60 25 10	60 20 5	50	40 5	7 1 1
Failu APL	25 25 50	25 50 95	40 75 90	40 80 95	90	- 95 100	100 100
i DPT Bor Gm (psi)	17 30 42	19 34 74	19 33 58	21 39 71	25 43 64	18 43 66	29 52 79
Mini DPT Bond Strength Rate Gm Failure Mo (in./min) (psi) APL CL	0.002 0.5 20						
Distance Aft of Aft Equator (in.)	7	٣	4	\$	9	7	œ

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¹Standard Deviation for Triplicate Tests

TABLE 37 (CONTINUED)

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MOTOR TC 30072 BOND STRENGTH AND LINER PROPERTIES IN AFT FLAP AREA, SEGMENT 64, 2-YEAR (1985) RESULTS

REVISION

	Mini	i DPT Bor	nd Stre	ngth		Liner	Liner	Liner C=0/C=C Ratios	Ratios
of Aft Equator (in.)	Rate om Failure Mod (in./min) (psi) APL CL	σm (psi)	Failu	Failure Mode (%) APL CL CL		Gel Fraction	Swell Ratio	C=C Stretching	C=C Vinyl
6	0.002 0.5 20	28 56 74	90 95 95	10 10 5	1 1 1	0.548 ± 0.01^{1}	2.17±0.04	Not Required	ired
10	0.002 0.5 20	30 51 78	- 90 100	50 10	20	0.543±0.01	2.11±0.06	0.367	0.073
11	0.002 0.5 20	26 51 73	- 95 100	40 5	9 1 1	0.550±0.04	2.16±0.14	Not Required	ired

1Standard Deviation for Triplicate Tests

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TABLE 38

MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT
IN FORWARD FLAP AREA, SEGMENT 1A1
2-YEAR (1985) RESULTS

			Re	elaxation	n Modulu	ıs (psi))
Distance From	Time From	Strain		Log	Time (mi		
Bondline (in.)	Cutting (hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
0.1	2.1	2.00	397	302	251	206	177
		2.00	455 426	<u>349</u>	291	242	212
		2.00	426	326	271	224	$\frac{212}{194}$
0.3	2.4	1.99	318	229	184	149	124
	2.8	2.00	323	238	191	156	134
		2.00	320	234	188	152	129
0.5	3.0	2.00	347	259	211	172	147
	3.1	2.00	347		208	172	150
		2.00	347	$\frac{253}{256}$	210	172	148
1.0	2.6	1.98	330	245	198	161	136
274	2.0	2.00	293		178	146	135
	2.0	1.99	312	$\frac{218}{232}$	188	154	$\overline{136}$
2.0	3.3	2.00	369	278	227	188	164
_,,	5.0	2.00	358	269	222	184	162
	3.0	$\frac{2.00}{2.00}$	364	$\frac{205}{274}$	$\frac{222}{224}$	186	163

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MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT IN FORWARD NIPPLE AREA, SEGMENT 1A 2-YEAR (1985) RESULTS

			Re	elaxatio	n Moduli	ıs (psi))_
Distance From	Time From	Strain		Log	Time (m:		
Bondline (in.)	Cutting (hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
0.1	3.1	2.00	306	235	198	168	148
	3.0	2.00	317	229	184	150	129
		2.00	312	232	191	159	138
0.3	3.4	2.00	330	248	201	163	1 37
	2.9	1.99	333	246	199	162	137
		2.00	332	247	200	162	1 37
0.5	3.7	1.99	410	309	256	210	182
	3.4	2.01	376	280	231	187	158
		2.00	393	294	244	198	170
1.0	3.0	2.00	404	305	254	210	182
	3.8	2.00	393	292	243	204	180
		2.00	398	298	248	207	181
2.0	3.3	1.98	268	189	149	118	98
	4.2	2.01	290	207	165	132	111
		$\frac{2.00}{2.00}$	$\frac{279}{279}$	198	157	125	104

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TABLE 40

MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT IN FORWARD EQUATOR AREA, SEGMENT 2L 2-YEAR (1985) RESULTS

	Distance From	Time From		Re	elaxatio			
Motor	Bondline	Cutting	Strain		Log '	Cime (mi	in)	
Location	(in.)	(hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
Area A	0.1	2.9	2.00	671	545	479	415	372
(Aft of		4.3	2.00	710	682	527	468	418
Equator, Between			2.00	691	614	503	411	395
Grounding	0.3	3.3	_	460	364	317	279	255
Straps)	0.3	3.7	_	467	382	333	294	266
Straps)		3.7		463	373	325	286	260
	0.5	3.7	1.99	493	400	346	302	271
			2.01	472	388	<u>337</u>	295	<u>270</u>
			2.00	482	394	341	298	270
	1.0	3.8	1.99	354	241	198	167	149
	1.0	4.5	1.99	494	363	306	260	229
		4.5	$\frac{1.99}{1.99}$	424	302	252	213	189
	2.0	4.0	2.01	406	317	269	238	212
	2.0	4.3	2.00	464	365	320	287	257
		4.3	$\frac{2.00}{2.00}$	435	$\frac{363}{341}$	294	262	234
Area B	0.1	4.6	_	586	492	436	383	349
(At Equator		3.5	_	606	496	433	374	335
Between Grounding	,	•		596	494	434	378	342
Straps)	0.3	5.0	1.99	443	458	411	368	338
Scraps)	0.3	3.9	2.02	545	362	315	275	247
		3.,	2.00	494	410	363	321	292
	0.5	3.5	2.00	439	350	301	260	233
		4.3	2.00	503	426	356	310	280
			2.00	471	388	328	285	256
	1.0	3.8	2.00	295	219	179	147	129
	1.0	3.4	2.00	402	339	270	233	208
		J.4	$\frac{2.00}{2.00}$	348	279	$\frac{270}{224}$	190	168
	2.0	4.2	2.00	342	260	218	184	164
	2.0	3.8	2.00	449	351	298	254	226
		3.0	$\frac{2.00}{2.00}$	395	305	258	219	194

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TABLE 40 (CONTINUED)

MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT IN FORWARD EQUATOR AREA, SEGMENT 2L 2-YEAR (1985) RESULTS

	Distance From	Time From		Re	elaxatio)
Motor	Bondline	Cutting	Strain		Log '	rime (m:	in)	
Location	(in.)	(hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
Area C	0.1	4.1	2.00	374	286	239	20 2	179
(Forward		2.5	2.00	449	351	297	255	228
of Equator in Flap			2.00	411	318	268	228	203
Area)	0.3	3.5	1.99	337	258	414	181	159
		2.8	2.01	354	273	229	194	171
			2.00	345	265	321	187	165
	0.5	3.8	1.99	316	248	208	177	156
		1.9	2.00	362	282	239	204	180
			1.99	339	265	223	190	168
	1.0	4.3	2.00	468	372	318	274	244
		2.3	2.00	455	362	310	266	235
		213	$\frac{2.00}{2.00}$	$\frac{461}{461}$	367	314	2 70	$\frac{235}{239}$
	2.0	2.1	2.00	247	183	152	127	112
		2.7	2.00	310	227	186	154	137
		2.,	$\frac{2.00}{2.00}$	$\frac{310}{278}$	$\frac{227}{205}$	$\frac{160}{169}$	$\frac{134}{140}$	$\frac{137}{124}$

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TABLE 41

MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT
IN BARREL AREA, SEGMENT 3A, BETWEEN AND UNDER GROUNDING STRAPS
2-YEAR (1985) RESULTS

	Distance From	Time From		D	elaxatio	n Maduli	is (noi)	
Motor	Bondline	Cutting	Strain			Time (m:		
Location	(in.)	(hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
Between Grounding	0.1	3.2 4.0	2.00 2.00	724 797	633 703	567 609	495 529	437 478
Straps		4.0	$\frac{2.00}{2.00}$	760	668	588	512	457
	0.3	3.6 2.3	2.00 2.00	621 621	516 533	456 460	404 402	366 358
		2.3	$\frac{2.00}{2.00}$	$\frac{621}{621}$	524	458	402	362
	0.5	3.8 2.8	1.99	474	375	325	281	252
		2.8	$\frac{2.00}{1.99}$	437 455	355 365	$\frac{312}{318}$	$\frac{258}{269}$	$\frac{226}{239}$
	1.0	3.3 2.9	2.01	468	351	281	228	177
		2.9	$\frac{2.00}{2.00}$	393 430	296 323	$\frac{249}{265}$	$\frac{206}{217}$	$\frac{183}{180}$
	2.0	3.7 3.5	<u>-</u>	450 437	337 324	278	234 213	205
		3.3	_	443	330	$\frac{262}{270}$	$\frac{213}{223}$	$\frac{179}{192}$
Under Grounding	0.1	3.0 3.9	1.99 1.98	1360 1550	1170 1310	1040 1170	930	859
Straps		3.9	1.98	1455	$\frac{1310}{1240}$	$\frac{1170}{1105}$	1010 970	<u>899</u> 879
	0.3	3.3 4.2	2.00 2.00	924 1020	774 861	684	608	563
		4.2	2.00	972	817	752 718	644 626	<u>569</u> 566
	0.5	3.6 2.9	1.99	869	748	665	597	536
		2.9	$\frac{2.01}{2.00}$	820 844	702 725	628 646	<u>554</u> 575	495 515
	1.0	2.8 3.2	2.00	623	506	428	366	319
		3. 4	$\frac{2.00}{2.00}$	575 599	451 478	3 <u>89</u> 408	$\frac{315}{340}$	$\frac{269}{294}$
	2.0	3.0	2.00	552	433	355	309	273
		3.5	$\frac{2.00}{2.00}$	$\frac{607}{579}$	<u>465</u> 449	384 375	$\frac{315}{312}$	$\frac{269}{271}$

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TABLE 42

MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT
IN AFT EQUATOR AREA, SEGMENT 51
2-YEAR (1985) RESULTS

	Distance From	Time From		R	elaxation	n Modul	ıs (psi))
Motor	Bondline	Cutting	Strain		Log	lime (m:	in)	
Location	(in.)	(hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
Area A	0.1	3.0	2.00	747	616	540	471	430
(Forward			2.00	790	<u>645</u>	562	496	430
of Equator, Between			2.00	768	630	551	483	430
Grounding	0.3	3.4	1.99	731	601	527	445	439
Straps)	0.3	3.3	2.00	868	745	638	559	488
Scraps)		3.3	$\frac{2.00}{2.00}$	799	673	582	502	463
	0.5	3.7	2.01	864	726	620	542	487
		3.6	2.00	951	794	696	607	539
			2.00	907	760	658	574	513
	1.0	3.0	1.99	713	563	476	402	354
	1.0	3.9	1.99	742	594	483	393	341
		3.7	$\frac{1.99}{1.99}$	727	578	479	397	347
	2.0	3.3	2.00	843	681	564	462	396
		3.2	2.00	750	594	514	442	386
			2.00	796	637	539	452	391
Area B	0.1	3.5	2.00	1500	1250	1090	925	816
(At Equator		4.1	2.00	1350	1110	956	795	683
Between Grounding	•		2.00	1425	1180	1023	860	749
Straps)	0.3	4.0	2.00	1140	927	793	673	598
561-7-7		3.5	2.00	1270	1260	851	900	592
			2.00	1205	1093	822	786	595
	0.5	3.3	2.00	1460	882	759	637	556
		3.7	2.00	1160	928	773	626	528
			2.00	1310	905	766	631	542
	1.0	3.6	2.00	894	686	554	443	370
		2.4	2.00	1010	794	654	544	463
			2.00	952	740	604	493	416
	2.0	3.9	2.00	912	727	613	527	456
		2.8	2.00	758	633	534	442	375
			2.00	835	680	573	484	415

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TABLE 42 (CONTINUED)

MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT IN AFT EQUATOR AREA, SEGMENT 51 2-YEAR (1985) RESULTS

	Distance From	Time From		Re	elaxatio	n_Modul	ıs (psi)
Motor	Bondline	Cutting	Strain		Log '	Time (m:	in)	
Location	(in.)	(hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
Area C (Aft of Equator, in Flap	0.1	3.0 3.7	$\frac{2.00}{2.00}$	941 891 916	757 677 717	654 549 601	544 394 469	478 351 414
Area)	0.3	3.0 4.0	$\frac{1.98}{2.00}$ $\frac{1.99}{1.99}$	745 <u>851</u> 798	606 642 624	504 519 511	424 404 414	365 325 345
	0.5	3.3 2.8	$\frac{2.01}{2.00}$	944 929 936	749 738 743	616 627 623	547 <u>526</u> 536	475 461 468
	1.0	3.6 3.1	$\frac{2.02}{1.99}$ $\frac{2.00}{2.00}$	1230 2160 1245	948 <u>951</u> 949	759 <u>747</u> 753	591 <u>556</u> 573	467 423 445
	2.0	3.4 3.4	$\frac{2.00}{2.00}$	786 1030 908	607 675 641	507 <u>546</u> 526	421 445 433	$\frac{350}{374}$ $\frac{362}{362}$

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TABLE 43

MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT
IN AFT FLAP AREA, SEGMENT 6A
2-YEAR (1985) RESULTS

	Distance From	Time From		Relaxation Modulus (psi) Log Time (min))	
Motor	Bondline	Cutting	Strain					
Location	(in.)	(hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
Area D	0.1	4.3 3.3	2.00	475	382	331	280	265
(End of Flap Near Nozzle)		3.3	$\frac{2.00}{2.00}$	331 394	254 318	210 270	175 228	$\frac{158}{212}$
	0.3	4.2	1.99	492	388	330	283	254
		3.7	$\frac{2.01}{2.00}$	<u>506</u> 499	404 396	342 336	287 285	$\frac{272}{263}$
	0.5	4.6	2.00	528	418	355	303	266
		2.6	$\frac{2.00}{2.00}$	506 517	404 411	342 349	287 295	272 269
	1.0	5.3	1.99	506	407	346	292	251
		2.9	$\frac{2.00}{1.99}$	<u>555</u>	444	<u>390</u>	348	326
	2.0	3.0	2.00	497	411	362	318	287
		-	$\frac{2.00}{2.00}$	524 511	$\frac{419}{415}$	$\frac{362}{362}$	$\frac{311}{315}$	282 285
Area E	0.1	3.7	2.00	563	455	392	340	309
(Apex Area)			$\frac{2.00}{2.00}$	600 582	$\frac{487}{471}$	410 401	389 365	351 330
	0.3	3.5	2.00	621	500	432	371	296
		2.9	$\frac{2.00}{2.00}$	537 579	$\frac{421}{461}$	355 394	305 338	270 283
	0.5	3.2	2.00	_	-	_	_	_
		3.6	$\frac{2.00}{2.00}$	573 573	457 457	<u>392</u> 392	334 334	301 301
	1.0	4.1	2.00	542	433	376	322	289
		4.0	$\frac{2.00}{2.00}$	<u>585</u> 564	<u>486</u> 460	426 401	380 351	$\frac{342}{316}$
	2.0	4.5	2.00	484	395	342	302	275
		3.9	$\frac{2.00}{2.00}$	606 545	501 448	$\frac{441}{392}$	389 346	$\frac{351}{313}$

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TABLE 43 (CONTINUED)

MOTOR TC 30072 STRESS RELAXATION GRADIENT OF PROPELLANT IN AFT FLAP AREA, SEGMENT 6A 2-YEAR (1985) RESULTS

	Distance From	Time From		R	elaxatio	n Moduli	us (psi))
Motor	Bondline	Cutting	Strain	Log Time (min)				
Location	(in.)	(hrs)	(%)	-0.93	-0.34	0.20	0.80	1.30
Area F	0.1	-	2.00	635	534	470	418	370
(Toward		2.9	2.00			_	_=_	_
Equator)			2.00	635	534	470	418	370
	0.3	-	2.00	680	639	528	449	398
		2.3	2.00	843	674	584	494	427
			2.00	762	657	556	472	413
	0.5	2.4	1.99	811	665	570	493	438
		2.7	2.01	860	696	614	522	471
			2.00	836	681	592	508	455
	1.0	2.1	2.01	799	658	571	492	439
		3.0	2.00	905	751	650	573	503
			2.00	852	705	611	533	471
	2.0	2.4	2.00	671	559	492	425	380
		2.2	2.00	745	602	526	466	414
			2.00	708	581	509	446	397

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TABLE 44

MOTOR TC 30072 STRESS RELAXATION OF V-45 INSULATION
IN FORWARD NIPPLE AND FORWARD AND AFT FLAP AREAS
2-YEAR (1985) RESULTS

		Re1	Relaxation Modulus (psi)			
	Strain		Log_Time	e (min)		
Motor Location	(%)	-0.34	0.20	0.80	1.30	
Forward Nipple						
Segment 1A	2.00 2.00 1.99 2.00	2760 2270 1990 2340	2250 2080 1830 2053	2060 1870 1660 1863	1920 1740 <u>1550</u> 1737	
Forward Flap						
Segment 1A1	2.00 1.98 2.00 2.00	2350 2320 2230 2300	2140 2120 2040 2100	1970 1950 1850 1923	1830 1820 1730 1793	
Aft Flap						
Segment 6A	2.00 1.99 <u>2.00</u> 2.00	3310 3040 <u>2540</u> 2963	3040 2760 2350 2717	2790 2480 2180 2483	2610 2280 2040 2310	

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TABLE 45

MOTOR TC 30072 STRESS RELAXATION OF V-45 INSULATION
IN FORWARD AND AFT EQUATOR AREAS BETWEEN GROUNDING STRAPS
2-YEAR (1985) RESULTS

		Rel	Relaxation Modulus (psi)		
	Strain		Log Tim	e (min)	
Motor Location	(%)	-0.34	0.20	0.80	1.30
Forward Equator:					
Area B	2.00	1080	997	919	866
(Near Case)	2.01	1250	1140	1050	987
	2.00	1280	1180	1100	1030
	2.00	1203	1106	1023	961
Area C	2.00	2410	2210	2030	1860
(Forward of	2.01	2580	2350	2140	2000
Equator, in	2.00	2630	2410	2210	2050
Flap Area)	2.00	2540	2323	2127	1970
Area A	2.01	1480	1340	1200	1100
(Aft of Equator)	2.00	1520	1390	1230	1140
<u>-</u>	2.01	1470	1330	1230	1140
	2.01	1490	1353	1220	1127
Aft Equator:					
Segment 5I	2.00	1070	979	900	827
Area B	2.01	1660	1520	1400	1330
	2.00	1320	1260	1150	1020
	2.00	1350	1253	1150	1059
Area C	2.00	2560	2330	2040	1830
(Aft of Equator	2.00	2090	1840	1580	1370
in Flap Area)	2.01	2570	2320	2070	1870
·	2.00	2407	2163	1897	1690
Area A	2.00	1470	1340	1220	1150
(Forward of	2.01	1740	1600	1430	1350
Equator)	2.00	1780	1630	1450	1340
-	2.00	1663	1523	1367	1280

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TABLE 46

MOTOR TC 30072 V-45 INSULATION PROPERTIES IN FORWARD NIPPLE AND AFT AND FORWARD FLAP AREAS 2-YEAR (1985) RESULTS

Motor Location	V-45 Moisture (%)	V-45 DOP (%)	V-45 Swell Ratio
Forward Nipple Segment IA	1.38 1.52 <u>1.66</u> 1.52	3.30 - - - 3.30	Not Required
Forward Flap Segment 1A1	$ \begin{array}{r} 1.24 \\ 1.22 \\ \underline{1.52} \\ \overline{1.33} \end{array} $	1.17 - - - 1.17	$ \begin{array}{r} 1.35 \\ 1.37 \\ \underline{1.35} \\ \overline{1.36} \end{array} $
Aft Flap Segment 6A	1.85 1.96 <u>1.62</u> 1.81	1.34 - - - 1.34	1.33 1.35 1.35

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TABLE 47

MOTOR TC 30072 V-45 INSULATION PROPERTIES IN FORWARD AND AFT EQUATOR AREAS BETWEEN GROUNDING STRAPS 2-YEAR (1985) RESULTS

Motor Location	V-45 Moisture (%)	V-45 DOP (%)	V-45 Swell Ratio
Forward Equator			
Segment 2L Area C (Forward of Equator, in Flap Area)	1.85 0.64 2.33 1.61	1.53 - - - 1.53	$ \begin{array}{c} 1.33 \\ 1.33 \\ \underline{1.33} \\ 1.33 \end{array} $
Area A (Aft of Equator, Between Grounding Straps)	1.39 1.49 <u>1.47</u> 1.45	3.11 - - - 3.11	1.33 1.37 <u>1.37</u> 1.36
Aft Equator			
Segment 5I Area C (Aft of Equator, in Flap Area)	0.96 1.09 1.21 1.08	1.96 - - - 1.96	$ \begin{array}{r} 1.35 \\ 1.34 \\ \hline 1.34 \\ \hline 1.34 \end{array} $
Area A (Forward of Equator, Between Grounding Straps)	1.08 1.10 <u>1.06</u> 1.08	1.78 - - - 1.78	1.37 1.35 1.36

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TABLE 48

MOTOR TC 30072 V-45 INSULATION PROPERTIES IN BARREL AREA BETWEEN AND UNDER GROUNDING STRAPS 2-YEAR (1985) RESULTS

Motor Location	V-45 Moisture (%)	v-45 pop (%)_	V-45 Swell <u>Ratio</u>
Segment 3A, Between Straps	0.91 0.71 <u>0.86</u> 0.83	Not Required	Not Required
Segment 3A, Under Straps	0.86 0.90 0.78 0.83	Not Required	Not Required

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